Contents lists available at ScienceDirect



Journal of Quantitative Spectroscopy and Radiative Transfer

journal homepage: www.elsevier.com/locate/jqsrt



Time-resolved Fourier transform infrared emission spectra of atomic Xenon: Newly measured Rydberg *g*-, *h*- and *i*-levels

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ARTICLE INFO

Keywords: Time-resolved Fourier-transform spectroscopy Infrared spectra Rydberg levels Xenon Atomic data

ABSTRACT

The time-resolved Fourier transform technique was employed to record the spectrum of neutral xenon (Xe I) within a distinct spectral range of 700–14000 cm^{-1} range. A complete series of up to one hundred scans were carried out and averaged to obtain a satisfactory signal-to-noise ratio with a resolution of 0.02 cm^{-1} , providing a detailed and high-quality representation of the xenon spectra. All existing observations of atomic Xe (1318 lines of which 111 are observed in this work for the first time) were included into the optimization procedure. As a result, we obtain an updated system of Xe I levels.

1. Introduction

Studying atomic Xe is important and relevant in various fields, including spectroscopy, radiative transfer, plasma diagnostics, laser physics, astrophysics, atomic physics, and potential technological applications. Xenon is also studied in the field of atomic physics, where it is used as a benchmark for theoretical calculations of atomic structure and interactions. The atomic Xe has potential applications in fields such as lighting, fluorescent displays, and plasma processing. Its unique properties, such as high ionization potential and low reactivity, make it a promising candidate for these applications.

Spectroscopic measurements on atomic Xe have been conducted for many years [1-5]. Broad understanding of atomic structure of Xe was first established in 1929 by Meggers [2] who photographed the Xe spectrum using a quartz-prism and a diffraction grating spectrometer in the wavenumber range from 9890 cm^{-1} to 29,050 cm^{-1} and reported 318 lines of neutral Xe. Further investigations in 1930 by Humphreys [3] extended the spectral range of observation to include both krypton and xenon. Humphreys employed a Fabry-Perot interferometer and glass discharge tubes as radiation sources to study the spectral range from 11,000 to 25,000 cm⁻¹. To improve the accuracy and precision of measurements, Humphreys and Meggers [6] re-examined the spectral range from 8000 to 30,000 cm⁻¹ using highresolving power grating spectrometers and an interferometer. Their work had a wavelength accuracy of approximately 0.01–0.02 Å. In 1934, Meggers and Humphreys [4] further improved the precision (uncertainty within 0.001 Å) by performing interference measurements on the natural xenon spectrum in the photographic region. This study

covered 132 transitions with wavenumbers ranging from 10,075 to 25,320 cm⁻¹. Subsequently, in 1935, Meggers [5] added 25 additional Xe lines in the infrared range of 7500 to 9500 cm⁻¹. Humphreys and Kostkowski [7] investigated the range from 5900 to 8500 cm⁻¹ using a high-resolution grating spectrometer with 15,000 lines per inch and a lead-sulfide photo-conducting diode. Humphreys summarized the results of his various measurements in a compilation [8]. Mishra et al. [9] recorded Xe I spectra excited in a microwave discharge using Fourier transform spectroscopy (FTS) with an unapodized instrumental resolution of 0.1 cm⁻¹ and estimated the absolute accuracy of the measured wavenumbers to be better than 0.003 cm⁻¹ for strong transitions.

To combine and generalize the findings from these diverse measurements, Saloman created a critical compilation [10] which serves as the primary source for Xe I lines listed at National Institute of Standards and Technology Atomic Spectra Database (NIST ASD) [11].

However, the NIST ASD Xe I linelist does not spread beyond wavelengths longer than 5.5 μ m, which is the InSb detector limit. Consequently, this linelist lacks infrared transitions involving Rydberg levels with high orbital momentum (l > 3), such as g-, h-, or i-levels. With liquid nitrogen cooled MCT (HgCdTe) detectors, the Fourier transform spectroscopy technique can be enhanced to observe transitions between these Rydberg levels in the mid-infrared domain, specifically below 1800 cm⁻¹.

The present study aims to investigate and report on these previously unobserved transitions, providing experimental energies of high–*l* Rydberg levels of neutral xenon. This research builds upon our previous

https://doi.org/10.1016/j.jqsrt.2024.108939

Received 29 June 2023; Received in revised form 13 February 2024; Accepted 13 February 2024 Available online 15 February 2024 0022-4073/© 2024 Elsevier Ltd. All rights reserved.

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studies of high-resolution infrared (IR) spectra of noble gas atoms [12–15]. In this study, we have measured 335 lines of atomic Xe in the spectral range of 700–14,000 cm⁻¹ using Fourier transform infrared spectroscopy with a spectral resolution of 0.02 cm⁻¹.

2. Experimental details

To measure the Xe spectra in the range from 700 to 14,000 cm^{-1} , we have applied two discharge methods:

- 1. Alternating current (AC) discharge with time-resolved Fourier transform (FT) spectroscopy (700–7900 cm⁻¹). Due to software compatibility, our time resolved system is limited up to 7900 cm⁻¹.
- 2. Microwave (MW) discharge without the time resolution technique (700–14,000 $\mbox{cm}^{-1}).$

In our experiments the natural xenon (mixture of nine stable isotopes of Xe) was used. As it is shown in Refs. [16-18], the hyperfine splitting of Xe I levels and the isotope shift of Xe I transitions are of order of (or less than) 1 GHz ≈ 0.033 cm⁻¹, so these effects are not observable at our spectral resolution. Note that Ref. [16] reports on absolute frequency measurements of two lines (transitions from the ground state to $8d[\frac{1}{2}]_1$ and $8d[\frac{3}{2}]_1$ in ¹³⁶Xe and one line (transition from the ground state to $7s'[\frac{1}{2}]_1$ in ¹³²Xe and measured isotope shifts of these lines in all isotopes present in natural xenon samples. From these measurements, one can derive the wavenumbers that should be observed in natural xenon, which was made by Saloman in his compilation [10]. For these three lines, which essentially define the connection of all excited level system to the ground level, we used Saloman's values. The VUV frequency-comb spectroscopy measurement [19] deals with 132 Xe isotope only. The isotope shift of this transition are needed for¹²⁹Xe and ¹³¹Xe are needed to adapt the results of Ozawa and Kobayashi [19] to the natural Xe mixture, so we did not include this high-accuracy measurement result into our optimization.

2.1. Time-resolved fourier transform infrared spectroscopy

To investigate chemical reactions and dynamic properties of molecules, radicals, and ions, time-resolved spectroscopy is an efficient technique. In our study, we employed a special approach called synchronous scanning Fourier transform (FT) technique for time-resolved spectra analysis, particularly for phenomena lasting from microseconds to milliseconds [20]. This technique involves initiating the reaction in a pulsed mode, *e. g.* using a laser, electric discharge (utilized in this experiment), electron bombardment, or a hollow cathode [21]. More exploration of the FT technique applied to molecular measurement can be found in our previous research publications [22,23].

The data acquisition was performed using a modified Bruker IFS 120 spectrometer located at the J. Heyrovský Institute of Physical Chemistry [24]. Once a sufficient amount of data and scans were acquired, the time-shifted interferograms were composed. The modified Bruker IFS 120 spectrometer, adapted for time-resolved measurements, generated the scan's initiating signal, as well as the fringe signals of the He-Ne laser. These signals functioned as the system's time standard. The additional electronic signals crucial for synchronizing the measurement process, such as the discharge trigger and the analog-to-digital (AD) sampling trigger, were produced by the Field Programmable Gate Array (FPGA, Altera).

During the pulse excitation, our experimental setup continuously recorded the signal from the detector while the interferometer's mirror was continuously scanning. The entire measurement process was synchronized with He-Ne laser fringes. Fig. 1 illustrates the chart diagram of our time resolution and data acquisition system, providing a description of the time parameters used in our experiments. We set a measurement window limit of 100 μ s, driven by the mirror speed of 10 kHz. The pulse width was specifically calibrated to 22 μ s. The data

acquisition process comprised 30 data points with 3 μ s offset after the beginning of the pulse. Each of the data points represents a complete recording across the entire spectral range at a distinct acquisition time. Data was acquired every 2nd microsecond, which covered a total acquisition window of 60 μ s. Thanks to these configurations, we were able to record 10 spectra during the active pulse duration and 20 additional spectra in the post-discharge pulse phase. Our setup enabled us to take up to 30 time-resolved spectra with the spectral resolution ranging between 0.15 cm⁻¹ and 0.02 cm⁻¹ in one measurement. The time resolution achieved was approximately 1 μ s, primarily limited by the bandwidth of the detector amplifier.

For more detailed information on the experimental setup, we refer to our previous papers [20,25,26].

2.2. Data acquisition

We employed two different methods to generate the xenon plasma in our experimental setup. The first method utilized a pulsed positive column discharge. A discharge tube with water-cooled stainless steel electrodes, measuring 20 cm in length and 12 mm in inner diameter, was filled with high-purity xenon gas (purity class 4.0: 99.990%). To achieve a strong emission spectrum, the xenon pressure was optimized at 0.5 torr. The discharge parameters applied across the electrodes were as follows: 1 kV voltage, 22 μ s pulse width, and 100 mA peak-to-peak current.

The second method involved a microwave discharge operating at 2.45 GHz, which was used to generate the xenon plasma [27]. In this case, an electrodeless discharge lamp (EDL) was utilized as the emission source. The EDL was a 10 mm diameter and 8 cm long sealed tube filled with 0.5 torr of xenon. The microwave power varied from 15 to 25 watts. The EDL was cooled with dry ice to reduce the heat generated during the discharge and further cool the source.

The emitted radiation from both plasma generation methods was focused into a Bruker IFS 120 Fourier transform spectrometer, covering the spectral range of 700–14,000 cm⁻¹. The instrument was equipped with a KBr beam splitter and an HgCdTe (MCT) detector for the 700– 2000 cm⁻¹ range, and a CaF₂ beam splitter and an InSb detector for the 2000–14,000 cm⁻¹ range. Different combinations of windows and lenses (a KBr window with a ZnSe lens and a CaF₂ window with a CaF₂ lens) were utilized depending on the spectral region of interest. Band pass interference filters (manufactured by Northumbria Optical Coatings Limited, UK) were used to improve the signal-to-noise ratio.

All the spectra were recorded with a non-apodized resolution of 0.02 cm^{-1} and a time resolution of $1-2 \,\mu$ s. The resulting matrix contains 30 time-shifted interferograms (1 or 2 microsecond time shift) with the 22 microsecond discharge pulse duration at the beginning of the data acquisition process. Our system not only enables the time-resolved spectra measurement, but also provides 30 observed spectra that can be averaged to improve the signal-to-noise ratio. These averaged spectra were used for the analysis of each spectral line. The complete experimental parameters applied to the entire data acquisition process are presented in Table 1.

2.3. Wavenumber calibration

The wavenumber scale of the spectrum was calibrated using spectral lines of several molecular and atomic species (N₂O, CO, H₂O, NH₃, and Xe I). Most of the spectra used for the calibration were measured in absorption (the only exceptions were the CO and Xe observed in emission). A cell filled with the calibration gas (pressure ~2 torr) was placed in the sample chamber of the spectrometer and the spectrum with the Xe discharge as the radiation source was measured. A few H₂O lines at the atmospheric pressure (outside the spectrometer) were also used. In the spectral range above 2000 cm⁻¹ an IR-lamp was utilized as an additional radiation source because of the low intensity of the discharge's black body radiation in this region. For the calibration



Fig. 1. Chart diagram of the time resolution and data acquisition system. Each measurement window was limited to 100 μ s because of 10 kHz mirror speed. Pulse width was set to 22 μ s. The data acquisition consisted of 30 acquisition points with 3 μ s offset, each point being a full spectrum in the whole spectral range at a specified time of acquisition. Acquisition was set to each 2nd microsecond, thus covering a 60- μ s acquisition window. Because of these particular settings, 10 spectra were recorded within the pulse duration and 20 spectra after the discharge pulse period.

I	ab	le	1	

Single-measurement spectral ranges and instrument configuration.

Spectral range (cm ⁻¹)	Method of discharge	Windows	Northumbria Optical Coatings Limited Filter specification	Detector	Beam splitter	Lens
700–1000	AC	KBr	WBP 3067	MCT	KBr	ZnSe
1000-1250	AC	KBr	WBP 3067	MCT	KBr	ZnSe
1250-1600	AC	KBr	WBP 3067	MCT	KBr	ZnSe
1600-2000	AC	CaF ₂	WBP 3067	InSb	CaF ₂	CaF ₂
2000-4000	AC	CaF ₂	LWP 3673	InSb	CaF ₂	CaF ₂
4000-5000	AC	CaF ₂	WBP 3834	InSb	CaF ₂	CaF ₂
5000-7700	AC	CaF ₂	WBP 4187	InSb	CaF ₂	CaF ₂
7700–14,000	EDL	CaF ₂	no filter	InSb	CaF ₂	CaF ₂

we used a set of spectra measured during the whole experimental campaign. More than 200 spectral lines were used for the calibration to cover the entire spectral range of this experiment. The spectral lines used for the calibration belong to the following vibration bands: N₂O (02⁰0–00⁰0, 10⁰1–00⁰0), CO (2–1, 4–2, 1–0, 3–1,), H₂O (010–000, 001–000), NH₃ (0100–0000, 0200–0100), and Xe I (lines listed in the NIST ASD [11]) for the spectral range up to 5000 cm⁻¹ and N₂O (20⁰1–00⁰0, 00⁰2–00⁰0), CO (4–2, 3–1), and Xe I (lines listed in the NIST ASD [11]) for the range 5000–12,000 cm⁻¹. The data used for the calibration were included in the supplementary online material. The high-precision reference wavenumbers of the above molecular lines were taken from the HITRAN database [28]. The typical uncertainties of the reference HITRAN wavenumbers are: $\Delta \nu_{\rm ref}(N_2O) \sim 0.001$ cm⁻¹, $\Delta \nu_{\rm ref}(CO) \sim 0.001$ cm⁻¹ $\Delta \nu_{\rm ref}(NH_3) \sim 0.0001$ cm⁻¹

The calibration was performed by linearly fitting ($W_{corrected} = W_{observed} - (\alpha * W_{obserbed} + \beta)$) the observed line positions to the reference high-precision wavenumber values from the HITRAN [28], HITEMP [29], and NIST ASD [11] databases (see Fig. 2). The obtained calibration factors were small, having little effect on the most of the resulting wavenumbers listed in Table 2. The wavenumber correction factors with their uncertainties are as follows:

- spectral range 800-5000 cm⁻¹: $\alpha = 3.00 \cdot 10^{-7}$, $\Delta \alpha = 1.27 \cdot 10^{-7}$; $\beta = -5.06 \cdot 10^{-3}$, $\Delta \beta = 2.01 \cdot 10^{-4}$
- spectral range 5000–12,000 cm⁻¹: $\alpha = 1.56 \cdot 10^{-7}$, $\Delta \alpha = 1.33 \cdot 10^{-7}$; $\beta = 3.28 \cdot 10^{-3}$, $\Delta \beta = 1.10 \cdot 10^{-3}$.

The error bars in Fig. 2 show the observed uncertainties,

$$\Delta v_{\rm obs} = \sqrt{(\Delta v_{\rm stat})^2 + (\Delta v_{\rm ref})^2},\tag{1}$$

where Δv_{ref} are the uncertainties of the reference line wavenumbers. The statistical uncertainties, Δv_{stat} , are supposed to be the maximal value: $\Delta v_{stat} = \max{\{\Delta v_{Brault}, \Delta v_{fit}\}}$, where Δv_{Brault} is determined by the general expression (2) for the line position error according to [30]:

$$\Delta v_{\text{Brault}} = \frac{W}{\text{SNR} N_{W}^{1/2}} \tag{2}$$

where SNR is signal-to-noise ratio, W is the full width at half maximum (FWHM) and N_W is the number of statistically-independent data points per W. The uncertainties Δv_{fit} are errors due to fitting the measured data arrays to a Lorentzian or Gaussian line profile. The fit and the estimation of the corresponding statistical uncertainties Δv_{fit} can be obtained using any software for data visualization (*e. g.*, Origin) or scientific calculation (*e. g.*, *Mathematica*).

Full uncertainties of the measured wavenumber were calculated by adding the observed (1) and calibration uncertainties in quadrature, $\Delta v = \sqrt{(\Delta v_{obs})^2 + (\Delta \alpha \cdot v)^2 + (\Delta \beta)^2}$, where α and β are the parameters obtained by fitting the wavenumber deviations of the reference lines (see Fig. 2).

For the wavelengths calibration several spectra recorded before as well as after the measurement of the spectra used for the analysis in this work. So that all the data are calibrated by two sets of the calibration parameters belonging to two spectral regions, 800-5000 and 5000-12,000 cm⁻¹.



Fig. 2. Differences between the observed and reference spectral line positions used for the wavenumber calibration. The various colors correspond to different species: green — N_2O , blue — H_2O , cyan — CO, magenta — NH_3 , and red — Xe I. The black line shows the fitted linear calibration function. Panel A and B show a single calibration plot split into two parts for better readability. Panel C is a separate calibration plot.



Fig. 3. 6h-7i and 6g-7h transitions lines near 815 cm⁻¹ in measured spectrum.

3. Results and discussion

As a result, 335 spectral lines of Xe I were detected in the entire spectral range of 700–14,000 cm⁻¹. Among these lines, 111 are identified for the first time, and most of these appeared in the spectral region below the 2500 cm⁻¹.

The observed and fitted spectral lines of the 6h-7i and 6g-7h transitions near the 815 cm⁻¹ spectral region are displayed in Fig. 3.

As an example, the time-resolved spectrum of the 5g-6h transitions of Xe I near 1340 cm⁻¹ is depicted in Fig. 4.

To obtain the line parameters, such as wavenumbers of the line positions, intensities and line widths, the lines measured in the AC discharge were fitted with Lorentzian profiles, and lines obtained in the microwave discharge were fitted with a Gaussian profile. For identification, we use the J_1l -coupling notation. For example, the notation $6p'[3/2]_1$ in Table 2 means $5p^5({}^2P_{1/2})6p^2[3/2]_1$ and the final term in such coupling scheme results from coupling the parent-level $J_1 = 1/2$ to



(a) The time profile of 5g-6h transitions in 1340-1360 cm⁻¹ spectral range.





(b) Lorentzian fitted profile for the observed line at 1353.8 cm⁻¹.

(c) Temporal decay of the 1353.8 cm⁻¹ line during the 22 microsecond time duration of the discharge pulse (1 μ s sampling method).

Fig. 4. The time-resolved spectra of Xe I near 1350 cm⁻¹ spectral range. Spectra were recorded with 22 μ s pulse width and 30 μ s data acquisition window. A small bump on the time profile curve (25 μ s) in Fig. 4(c) is probably caused by multi-level deexcitation via various relaxation paths, thus resulting in to secondary excitations.

the orbital angular momentum of the 6*p* electron to obtain the resultant K = 3/2 (the *K* value is enclosed in brackets). The spin of the external electron (2S + 1 = 2) is then coupled with the *K* angular momentum to obtain a pair of *J* values, $J = K \pm 1/2$ (see the Notations for Different Coupling Schemes Section of Ref. [31]). Table 2 lists all our observed and classified lines involving transitions between $5p^5(2P_{1,2,2})nl^2[K]_J$ levels with n = 4–9. The measurements were performed in different spectral ranges: 700–1000, 1000–1200, 1200–1800, 1800–2000, 2000–4000, 4000–5000, 5000–7700, 7700–14,000 cm⁻¹. The arbitrary units of intensity I_{ki} are valid only within the same spectral range because we used different combinations of detectors and optics to cover the entire range (see Table 1).

The uncertainties (on the level of one standard deviation) of the measured lines presented in Table 2 are given in parentheses (for example, 123.4(56) means 123.4 ± 5.6).

The last column in Table 2 presents the wavenumbers of Xe I obtained from previous measurements. The uncertainties in wavenumbers for the measured values are taken from Table 3 of Saloman [10]. In general, our results are in agreement with those from prior studies, taking into account the reported uncertainties.

To extract the energies of Xe I levels from the measured line wavenumbers we used the LOPT program [38]. This software executes a least-square optimization of the level energies to minimize the

total of squared differences between the observed and Ritz values. The precision of the fit is strongly correlated with the quality and fullness of the spectral lines input set for the fitting process. Thus, it is important to gather as much spectral data from literature as possible for xenon atom, limited by laboratory observations only (the theoretical calculations were not included). In our study, we compiled spectral data from various literature sources [4–9,16,32–35,37,39–45] for the Xe atom. These data comprise 1318 lines; the complete list of lines with classifications, uncertainties, observed—Ritz differences and references is available as a supplementary online material.

The internal consistency of our measured wavenumbers presented in Table 2 was inspected by calculating the reduced residuals, $R_i = (\sigma_{obs,i} - \sigma_{calc,i})/u_i$. For a specific line *i*, this metric is computed as the difference between the observed wavenumber $(\sigma_{obs,i})$ and the computed Ritz wavenumber $(\sigma_{calc,i})$, normalized by the uncertainty of the observed wavenumber (u_i) . The reduced residuals R_i are plotted as a function of the corresponding normal order statistic medians which are defined as $G(U_i)$ [46]. Here U_i represents the expected value of the *i*th order statistic in a array of size *n* from a uniform distribution on the interval [0,1]. The function *G* is the inverse of the standard normal cumulative distribution function (CDF). So, the normal probability plot is constructed by plotting the reduced residuals R_i against the corresponding $G(U_i)$ values. $G(U_i)$ in our case depends only on number

Table 2

Xe IR line wavenumbers v_{ki} , intensities I_{ki} , signal-to-noise ratios (SNR) and full widths at half-maxima (FWHM). The measurements were performed in different spectral ranges: 700–1000, 1000–1200, 1200–1800, 1800–2000, 2000–4000, 4000–5000, 5000–7700, 7700–14000 cm⁻¹. The arbitrary units of intensity are valid only within the same spectral range. Description of literature abbreviations in column 'Other work': [L1975] [32]; [L234] [33]; [L2228] [8]; [L4227c110] [34]; [L9760] [9]; [L7384] [7]; [L7293] [5]; [L7292] [4]; [L4739] [6]; [L4085] [35]; [L4211c2] [36]; [L7449] [37].

v_{ki} (cm ⁻¹)	I _{ki}	SNR	FWHM	Identification	Other work
	(arb. u.)		(cm ⁻¹)		(if any)
732.070(15)	2.46×10^{6}	10.2	0.077(13)	$7d[7/2]_3 - 5f[9/2]_4$	
742.283(10)	1.22×10^{5}	3.18	0.076(20)	$7d[5/2]_2 - 5f[7/2]_3$	
774.148(22)	2.86×10^{6}	5.42	0.060(21)	$6p[3/2]_2 - 5d[1/2]_1$	
781.336(11)	1.15×10^{5}	3.40	0.056(21)	$7p[1/2]_1-6d[3/2]_2$	
792.008(13)	1.44×10^{5}	3.20	0.141(27)	$9s[3/2]_2 - 9p[3/2]_2$	
807.894(17)	9.37×10^{5}	2.90	0.149(38)	6h[11/2]-7i[13/2]	
809.041(9)	4.07×10^{6}	2.60	0.213(22)	6h[9/2]-7i[11/2]	
811.598(23)	1.82×10^{6}	7.45	0.082(63)	6h[13/2]-7i[15/2]	
812.705(30)	1.34×10^{6}	5.50	0.119(28)	6h[7/2]-7i[9/2]	
815.223(19)	1.19×10^{6}	6.13	0.063(18)	$6p[3/2]_1 - 5d[1/2]_0$	
816.350(12)	1.58×10^{6}	5.43	0.163(18)	6g[11/2]-7h[13/2]	
817.281(14)	9.54×10^{5}	7.44	0.053(12)	$6d[3/2]_1 - 4f[3/2]_2$	
818.799(27)	8.35×10^{4}	2.41	0.128(89)	6g[5/2]-7h[7/2]	
848.069(5)	1.02×10^{7}	21.2	0.061(5)	$7p[3/2]_2 - 6d[5/2]_3$	
864.137(7)	2.12×10^{6}	14.9	0.077(7)	$6p'[3/2]_1 - 6d[5/2]_2$	
877.893(5)	3.65×10^{6}	18.1	0.056(5)	$6d[3/2]_1 - 4f[5/2]_2$	
891.579(5)	3.98×10^{6}	23.1	0.061(5)	$7p[5/2]_2 - 6d[5/2]_2$	
912.031(30)	9.23×10^5	3.69	0.054(28)	$5f[9/2]_4 - 8d[7/2]_3$	
918.614(8)	8.18×10^4	4.16	0.063(17)	$5f[7/2]_3 - 8d[5/2]_2$	
923.442(17)	1.43×10^{6}	6.31	0.082(15)	$5d'[3/2]_2 - 8p[3/2]_2$	
932.542(5)	1.34×10^{7}	37.9	0.068(2)	$7d[7/2]_4 - 5f[9/2]_5$	
949.086(21)	9.46×10^{5}	6.78	0.096(20)	$5f[7/2]_4 - 8d[5/2]_3$	
1065.359(7)	1.14×10^{4}	5.96	0.051(16)	$7p[5/2]_3-6d[5/2]_3$	
1072.371(3)	5.20×10^{4}	9.51	0.056(11)	$6s'[1/2]_0 - 6p[1/2]_1$	
1110.281(5)	4.76×10^{5}	6.97	0.078(8)	$6p[3/2]_2 - 5d[3/2]_2$	
1133.300(3)	1.62×10^{4}	8.53	0.048(13)	$8p[5/2]_3 - 9s[3/2]_2$	
1189.901(5)	1.52×10^{4}	10.1	0.049(10)	$7p[1/2]_0-6d[3/2]_1$	
1287 500(4)	5.40×10^5	15.2	0.065(15)	7p[3/2] 6d[3/2]	
1207.355(4)	1.22×10^{6}	22.0	0.003(13)	$p_{1}(3/2)_{1} = 0u_{1}(3/2)_{1}$	
1206.920(9)	1.22×10^{5}	16.1	0.027(2)	$6d[5/2]_1 = 6p[5/2]_2$	
1341 044(5)	1.10×10^{6}	20.1	0.058(5)	$5a[9/2]_{3}$ -+ $f[9/2]_{4}$	
1345 730(5)	1.10×10^{6}	29.1	0.052(5)	5g[7/2]=6h[9/2]	
1348 740(5)	8.19×10^5	17.9	0.046(5)	8s[3/2] - 8n[1/2]	
1353 861(4)	1.94×10^{6}	31.5	0.043(3)	$5_{g}[11/2]_{2} = 6_{h}[13/2]$	
1358 082(6)	4.93×10^{5}	9.85	0.035(5)	$5g[5/2]_{2}=6h[7/2]_{2}$	
1358 297(7)	3.90×10^5	7 48	0.039(6)	$5g[5/2]_3 = 6h[7/2]_4$	
1364 950(6)	3.36×10^4	8.05	0.083(18)	$5f[7/2]_{-6g[9/2]_{-}}$	
1365.030(8)	7.90×10^{3}	5.22	0.030(17)	$5f[7/2]_{2} = 6g[9/2]_{4}$	
1366.717(3)	3.51×10^{6}	17.6	0.035(3)	$6p[3/2]_{-5d}[3/2]_{-5d}$	
1372.509(12)	2.74×10^{5}	8.05	0.044(11)	$6d[5/2]_2 - 4f[5/2]_2$	
1378.249(4)	2.81×10^{4}	7.17	0.039(16)	$5f[5/2]_2-6g[7/2]_3$	
1380.746(5)	1.67×10^{4}	7.39	0.045(11)	$5f[5/2]_3-6g[7/2]_4$	
1396.831(11)	2.68×10^{5}	8.65	0.058(10)	$5f[9/2]_4-6g[11/2]_5$	
1397.559(8)	3.58×10^{5}	8.74	0.041(7)	$5f[9/2]_5-6g[11/2]_6$	
1400.639(6)	5.56×10^{5}	15.2	0.035(6)	$8s[3/2]_1 - 8p[3/2]_1$	
1405.350(15)	1.51×10^{5}	6.23	0.028(13)	$5f[3/2]_2-6g[5/2]_3$	
1409.570(2)	4.02×10^{6}	44.5	0.029(2)	$6d[5/2]_{3}-4f[7/2]_{4}$	
1438.483(8)	3.16×10^{5}	10.4	0.033(7)	8s[3/2] ₁ -8p[3/2] ₂	
1460.411(4)	1.74×10^{6}	18.8	0.045(3)	8s[3/2] ₂ -8p[5/2] ₃	
1566.381(2)	2.91×10^{4}	24.6	0.025(2)	8s[3/2] ₂ -8p[3/2] ₂	
1584.281(2)	3.28×10^{5}	40.0	0.022(2)	$4f[9/2]_5 - 7d[7/2]_4$	
1666.806(2)	7.30×10^{4}	26.0	0.023(11)	$6d[5/2]_{2} - 4f[5/2]_{2}$	
1700.793(2)	2.44×10^{5}	9.06	0.024(6)	$6d[5/2]_2 = 4f[7/2]_2$	
1784.623(3)	2.00×10^{5}	5.51	0.027(10)	$4f[9/2]_{4} - 7d[7/2]_{2}$	
1789.468(4)	2.46×10^{5}	3.97	0.036(12)	$4f[7/2]_4 - 7d[5/2]_2$	
1793.568(2)	6.71×10^{7}	10.2	0.032(2)	$6p[5/2]_3-5d[7/2]_4$	
1836.616(2)	4.61×10^{6}	15.5	0.029(2)	$6d[7/2]_3 - 4f[9/2]_4$	1836.64(13) [L1975]
1866.820(2)	2.42×10^{5}	7.47	0.022(7)	$6p[5/2]_2 - 5d[1/2]_1$	
1919.157(2)	6.02×10^{5}	6.70	0.026(8)	$6d[7/2]_3 - 4f[7/2]_3$	1919.20(15) [L1975]
1919.238(11)	8.51×10^{5}	4.65	0.049(18)	$6d[7/2]_3 - 4f[7/2]_4$	1919.20(15) [L1975]
1948 958(10)	2.95×10^5	6.20	0.036(9)	6d[7/2] = 4f[9/2]	1949 00(11) [11075]
1961 369(19)	2.95×10^{4}	5.20	0.026(18)	$8n[5/2]_{$	1961 39(15) [I19/5]
1999 070(13)	6.31×10^4	5.86	0.037(12)	$8n[3/2]_{-8d[5/2]}$	1999 13(16) [11975]
2027 421(17)	7.42×10^4	5.22	0.037(17)	$6s'[1/2]_2 - 6n[3/2]$	2027 46(12) [11975]
2032 441(9)	540×10^5	5.48	0.050(8)	$6d[7/2]_{-4}f[7/2]$	2032 46(17) [11975]
2068 865(11)	3.69×10^5	7 89	0.047(11)	$8n[5/2]_{a} = 8d[7/2]_{a}$	2068 85(17) [11975]
2074 723(12)	9.55×10^4	4 95	0.051(11)	$8n[1/2]_{2} = 8d[1/2]_{3}$	2075 06(17) [11975]
2090 170(11)	1.92×10^{5}	4 70	0.061(9)	$7n[1/2]_{a}=8s[3/2]_{a}$	2090 20(17) [11975]
(11)	1.27.10		0.001())	· PL-/ 2]0 03[3/ 2]]	

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v_{ki} (cm ⁻¹)	I _{ki} (arb. u.)	SNR	FWHM (cm ⁻¹)	Identification	Other work (if any)
2118.039(10)	4.50×10^{5}	4.90	0.052(9)	$8p[5/2]_2 - 8d[5/2]_2$	2118.07(18) [L1975]
2140.972(7)	6.54×10^{5}	6.48	0.062(6)	$6d[3/2]_2 - 4f[3/2]_2$	2141.03(18) [L1975]
2154.324(6)	1.32×10^{5}	8.15	0.035(6)	5g[7/2]-7h[9/2]	
2164.025(6)	9.87×10^{4}	8.59	0.023(5)	5g[11/2]-7h[13/2]	
2168.767(9)	3.84×10^{5}	8.73	0.047(8)	$6p'[1/2]_1 - 5d'[3/2]_2$	2168.79(19) [L1975]
2187.874(11)	7.56×10^{5}	4.73	0.054(9)	$7p[3/2]_1 - 8s[3/2]_1$	2187.90(19) [L1975]
2198.622(12)	3.94×10^{6}	4.61	0.054(10)	$6d[3/2]_2 - 4f[5/2]_3$	2168.68(15) [L1975]
201.584(10)	1.74×10^{5}	6.62	0.037(9)	$6d[3/2]_2 - 4f[5/2]_2$	2201.58(19) [L1975]
2202.949(13)	1.91×10^{5}	6.97	0.053(13)	$6p[5/2]_2 - 5d[3/2]_2$	2202.97(10) [L1975]
2245.935(9)	2.74×10^{5}	7.23	0.056(8)	$7p[3/2]_2 - 8s[3/2]_1$	2246.0(2) [L1975]
2268.142(17)	1.14×10^{5}	4.31	0.041(4)	$5d'[5/2]_2 - 5f[7/2]_3$	2268.3(2) [L1975]
268.273(17)	1.17×10^{5}	4.69	0.053(3)	$6p'[1/2]_{0} - 7d[1/2]_{1}$	2268.3(2) [L1975]
290.004(9)	3.97×10^{5}	4.65	0.065(6)	$6d[1/2]_1 - 4f[3/2]_1$	2290.01(21) [L1975]
299.665(7)	7.45×10^{5}	5.68	0.070(5)	$6d[1/2]_1 - 4f[3/2]_2$	2299.66(16) [L1975]
300.904(14)	2.48×10^{4}	5.09	0.044(13)	$6d[3/2]_1 - 8p[3/2]_1$	2300.9(2) [L1975]
2335 328(9)	1.49×10^{6}	6.78	0.055(8)	$7n[5/2]_{2} = 8s[3/2]_{2}$	2335 31(16) [L1975]
348 758(8)	5.14×10^5	6 55	0.068(6)	$6d[1/2]_{-4}f[3/2]_{-4}$	2348 80(17) [L1975]
360 277(9)	1.10×10^5	5.61	0.049(7)	$6d[1/2]_0 = 4f[5/2]_1$	2360 3(2) [L1975]
408 114(20)	3.47×10^5	4 31	0.078(19)	7n[3/2] = 5d'[5/2]	2000.0(2) [H1970] 2408 13(16) [L1975]
425 421(18)	3.77×10^4	4 1 4	0.059(16)	6n'[3/2] = 8n[3/2]	2425 41(24) [L1975]
452 862(10)	3.12×10^{5}	 4 QA	0.053(10)	7n[5/2] - 8s[2/2]	2452 84(6) [1 224]
466 164(15)	5.15×10^{-1}	7.24	0.033(0)	$p_{1} p_{2} p_{3} p_{2} p_{3} p_{3$	2732.04(0) [L234] 9466 19(94) [L1075]
497 117(10)	1.24×10^{5}	5.4Z	0.031(13)	$p_{1} p_{2} p_{3} p_{3$	2700.13(24) [L19/5] 2407 12(4) [1 224]
HOF 619(9)	3.11 X 10 ²	5.01	0.000(9)	$(s_1)/2_1 - (p_1)/2_1$	2407.12(0) [L234]
493.012(8)	2.80 × 10 ⁵	5.70	0.089(4)	$4J[//2]_4 - 5g[//2]_4$	2495.59(6) [L234]
493.704(22)	2.05×10^{-3}	4.41	0.082(20)	$4J[//2]_3 - 5g[//2]_3$	2495.59(6) [L234]
501.915(13)	8.60 × 10 ⁴	3.05	0.053(10)	$4f[7/2]_4 - 5g[9/2]_5$	2502.06(6) [L234]
501.997(87)	3.93 × 10 ⁴	2.90	0.036(84)	$4f[7/2]_3-5g[9/2]_4$	2502.06(6) [L234]
502.130(7)	2.36×10^{3}	9.15	0.056(7)	$6p[1/2]_1 - 5d[1/2]_0$	2502.15(6) [L234]
511.232(11)	4.84×10^{3}	6.81	0.076(10)	$4f[5/2]_2 - 5g[5/2]_2$	2511.18(6) [L234]
514.405(8)	8.21×10^{3}	5.14	0.083(4)	$4f[5/2]_3 - 5g[5/2]_3$	2514.45(6) [L234]
522.977(10)	3.15×10^{5}	5.25	0.053(8)	$6d[3/2]_1 - 8p[1/2]_0$	2523.0(3) [L1975]
529.697(10)	5.69×10^{6}	4.87	0.056(8)	$4f[5/2]_2 - 5g[7/2]_3$	2529.73(6) [L234]
532.656(10)	7.99×10^{6}	4.87	0.057(8)	$4f[5/2]_3 - 5g[7/2]_4$	2532.68(6) [L234]
553.309(12)	3.49×10^{5}	4.97	0.055(11)	$6p'[3/2]_1 - 8s[3/2]_1$	2553.292(65) [L234]
565.854(9)	1.01×10^{7}	8.42	0.052(8)	$4f[9/2]_4 - 5g[11/2]_5$	2565.87(7) [L234]
566.708(13)	1.39×10^{7}	10.8	0.059(13)	$4f[9/2]_5 - 5g[11/2]_6$	2566.76(7) [L234]
567.381(15)	6.87×10^{6}	5.75	0.051(14)	$6p[5/2]_3 - 5d[7/2]_3$	2567.368(66) [L234]
572.054(10)	1.30×10^{6}	4.54	0.057(8)	$4f[3/2]_2 - 5g[5/2]_3$	2572.10(7) [L234]
580.753(9)	7.35×10^{5}	6.86	0.057(7)	$7p[5/2]_2 - 8s[3/2]_1$	2580.738(67) [L234]
581.508(9)	8.33×10^{5}	4.88	0.059(7)	$4f[3/2]_1 - 5g[5/2]_2$	2581.46(7) [L234]
584.211(10)	5.91×10^{5}	4.73	0.061(7)	$6p'[3/2]_2 - 5d'[5/2]_3$	2584.190(67) [L234]
584.557(13)	1.16×10^{5}	3.35	0.057(10)	$4f[9/2]_4 - 5g[9/2]_4$	2584.60(7) [L234]
585.403(7)	1.82×10^{5}	6.50	0.069(5)	$4f[9/2]_5 - 5g[9/2]_5$	2585.39(7) [L234]
596.945(24)	3.73×10^{4}	4.21	0.10(22)	$8s[3/2]_2 - 5f[5/2]_3$	2596.8(3) [L1975]
683.444(80)	4.48×10^{4}	5.04	0.066(18)	$7p[5/2]_3 - 5d'[5/2]_2$	2683.5(3) [L1975]
713.049(10)	4.87×10^{5}	4.74	0.056(8)	$6p[3/2]_2 - 5d[5/2]_2$	2713.1(2) [L1975]
717.473(7)	3.49×10^{6}	6.58	0.064(6)	$6p[1/2]_1 - 5d[1/2]_1$	2717.48(7) [L1975]
730.382(11)	2.42×10^{4}	7.15	0.045(11)	$6d[5/2]_2 - 8p[5/2]_2$	2730.4(3) [L1975]
738.355(7)	2.91×10^{6}	5.46	0.081(3)	$7s[3/2]_{2} - 7p[1/2]_{1}$	2738.34(8) [L1975]
759.252(6)	1.08×10^{5}	17.2	0.061(5)	$6s'[1/2]_0 - 6p[3/2]_1$	2759.26 [L2228]
760.978(12)	3.73×10^{5}	12.3	0.060(11)	$7p[3/2]_2 - 5d'[3/2]_2$	2760.97 [1.2228]
836.350(9)	2.72×10^{5}	6.12	0.067(8)	$6d[5/2]_2 - 8p[3/2]_2$	2836.36 [L2228]
350.640(9)	3.68×10^{7}	6.97	0.056(8)	$6p[5/2]_{2} = 5d[7/2]_{2}$	
877 410(7)	7.87×10^5	6.24	0.066(6)	$7n[1/2]_{-8}s[3/2]_{-1}$	2877 41 [1.2228]
011 664(0)	3.38×10^{6}	4 72	0.061(7)	7s[3/2] - 7r[5/2]	2012 06(85)[14227c11
022 015(16)	1.10×10^5	6.91	0.001(7)	6s'[1/2] = 6p[1/2]	2022 02 [12228]
020 111(12)	1.19×10^{5}	4.82	0.050(13)	$7_{c}[2/2] - 6_{r}/[2/2]$	2933.92 [L2226]
060 401(0)	4.20×10^{7}	7.05	0.059(11)	$(3[3/2]_1 - 6p[3/2]_1$	2939.11 [L2220]
09.401(0)	1.77×10^{-2}	7.23	0.030(7)	6d(5/2) = 5u(5/2) = 6d(5/2)	2078 26 [1 2228]
015 307(10)	2.37×10 2.27 $\sim 10^5$	5.02	0.029(17)	$7n[1/2] - 9p[3/2]_2$	3005 30 [13339]
JUJ.JU/(12)	2.37 × 10 ⁶	5.85	0.056(11)	$p_{1}^{2}_{21} = \delta_{2}^{2}_{21}^{2}_{21}$	3003.30 [L2228]
00.000(0)	3.00 × 10 ⁵	0.40	0.000(0)	$0p_{[1/2]_1} - 3a_{[3/2]_2}$	2000 01 [1 0000]
J07.804(11)	2.89 × 10°	4.09	0.058(9)	$0a_{13}/2_{12}-8p_{13}/2_{11}$	3087.81 [L2228]
095./90(19)	2.66 × 10 ³	4.52	0.051(18)	$p_{[5/2]_2} - 5d' [3/2]_2$	3095.79 [L2228]
162.903(10)	$4.80 \times 10^{\circ}$	4.99	0.055(9)	$[s_13/2]_2 - [p_15/2]_2$	3162.91 [L2228]
190.345(10)	5.27×10^{3}	6.21	0.066(8)	$[s_{3/2}]_{2}-6p'[3/2]_{1}$	3190.35 [L2228]
196.471(9)	5.33×10^{5}	7.04	0.057(8)	$6d[7/2]_3 - 8p[5/2]_2$	3196.47 [L2228]
217.739(9)	4.17×10^{7}	6.64	0.056(8)	$6p[3/2]_2 - 5d[5/2]_3$	
240.056(24)	8.42×10^{4}	3.99	0.070(22)	$6d[7/2]_3 - 8p[5/2]_3$	3240.06 [L2228]
246.482(10)	4.52×10^{6}	4.95	0.057(8)	$7s[3/2]_1 - 7p[3/2]_2$	3246.48 [L2228]
277.353(18)	2.62×10^{5}	5.22	0.049(17)	$7p[5/2]_3 - 5d'[5/2]_3$	3277.36 [L2228]
280.436(7)	2.49×10^{7}	7.43	0.058(6)	$7s[3/2]_2 - 7p[5/2]_3$	
286.034(17)	1.91×10^{5}	4.05	0.053(15)	$7p[1/2]_0 - 7d[1/2]_1$	3286.03 [L2228]
304.543(8)	4.10×10^{6}	6.88	0.061(7)	$7s[3/2]_1 - 7p[3/2]_1$	3304.54 [L2228]
330.006(17)	1.22×10^{5}	5.58	0.057(16)	8s[3/2] ₂ -9p[5/2] ₃	3329.99 [L2228]
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μ_{1} (m ²) μ_{1} (m ²) SNE PNUL (m ²) Identified Other was (if any) 3324.05(1) 2.6.8.10 ² 5.46 0.09(9) (61/2)-(41/2)-(41/2), (17/2)-(41/2), 3352.25(1) 3352	Table 2 (continued).					
(a^{h}, a) $(a^{m})^{h}$ (a^{m})	$v_{ki} ({\rm cm}^{-1})$	I_{ki}	SNR	FWHM	Identification	Other work
3334 0821)2.8.4 105.4.60.9690417/1_4.15/17/2_435.4.9 1L22813355 356101.9.8 10"4.3.20.00714)417/1_4.15/17/2_435.3.5 122313355 357101.9.8 10"5.30.00813717/1_4.15/17/2_135.3.5 122313355 357101.9.8 10"5.30.08513717/1_7.15/17/2_1340.24 122313354 35711.9.8 10"5.30.08513717/1_7.15/17/2_1340.24 12231341 4001.9.8 10"5.30.08510717/1_7.15/17/2_1340.24 12231341 4005.30.08510717/1_7.15/17/2_1340.24 12231335 358101.9.8 10"5.30.08501717/1_7.15/17/2_1357.5 112231335 358105.9.8 10"5.90.00901471/1_7.15/17/2_1355.7 112231335 358105.9.8 10"5.9.8 10"6.90.00901471/1_7.15/17/2_1355.7 112231335 358105.9.8 10"5.9.8 10"6.90.00901471/1_7.15/17/2_1355.7 112231355 358105.9.8 10"6.9.90.00901471/1_7.15/17/2_1355.7 112231355 358105.9.8 10"6.9.90.00901471/1_7.15/17/2_1357.5 112231355 3591105.9.8 10"6.90.00901471/1_7.15/17/2_1357.5 112231355 3591105.9.8 10"5.7.80.00901471/1_7.15/17/2_1377.5 112231355 3591105.9.8 10"5.7.80.00901471/1_7.15/17/2_1377.5 112231355 3591105.9.8 10"5.7.80.00901471/1_7.1		(arb. u.)		(cm ⁻¹)		(if any)
383.358/00 1.0 × 10 ¹ 7.26 0.056/71 0.071/21-091/21 371.871 387.8710 6.8 × 10 ¹ 0.12 0.00110 0.011/21-011/21 371.871 387.8710 6.8 × 10 ¹ 0.12 0.00110 0.011/21-011/21 371.871 387.8710 7.0 × 10 ¹ 5.41 0.07960 710/21-011/21 341.2221 392.8410 7.0 × 10 ¹ 5.41 0.06810 710/21-011/21 341.2221 340.72017 5.44 0.0810 710/21-011/21 341.2221 340.72017 5.44 0.0810 710/21-011/21 341.2221 340.72017 5.34 0.0810 710/21-011/21 352.5610 350.55001 2.1 × 10 ⁻² 6.21 0.0010 710/21-011/21 352.5612 350.550010 2.1 × 10 ⁻² 6.53 0.00210 611/21-611/21 353.5122 350.550010 2.1 × 10 ⁻² 6.53 0.00210 611/21-611/21 353.5122 350.550010 2.5 × 10 ⁻² 6.64 0.00210 611/21-611/21 353.5122 350.550010 7.5 × 10 ⁻² 6.64 0.00210 611/21-611/21 353.5122 350.550010 7.5 × 10 ⁻² 6.64 0.00210 611/21-61/21 353.51122 <td>3334.082(11)</td> <td>2.62×10^{5}</td> <td>5.48</td> <td>0.069(9)</td> <td>$6d[3/2]_1 - 5f[3/2]_2$</td> <td>3334.09 [L2228]</td>	3334.082(11)	2.62×10^{5}	5.48	0.069(9)	$6d[3/2]_1 - 5f[3/2]_2$	3334.09 [L2228]
3355.97(4); 8.77.10" 4.12 0.071.4) 4.1972,-47172, 337.18 [[223] 3357.271807(8) 6.88.10" 4.57 0.08518) 7.1471,-1471,71, 336.37 [[223] 3357.27197(8) 2.64.10" 5.34 0.09701 7.1472,-1471,71, 346.27 [[223] 3457.27107(8) 2.64.10" 5.38 0.08518) 7.1472,-1471,71, 346.27 [[223] 3467.27107(8) 2.53.11" 6.23 0.08618) 7.1472,-1471,71, 346.27 [[223] 3520.375107 3.53.11" 1.5 0.02413) 7.1472,-1471,71, 352.25 [[1223] 3520.375107 3.54.11" 1.0 0.02113) 6.1172,-1471,71, 350.25 [[1223] 3520.37510 3.54.11" 1.0 0.02113) 6.1172,-1471,71, 350.25 [[1223] 3520.37510 3.54.11" 0.44 0.04133 6.1172,-1471,71, 350.25 [[1223] 3520.37510 3.54.11" 3.64 0.04133 6.1172,-1471,71, 350.25 [[1223] 354.26207 3.54.11" 3.64 0.04133 6.1172,-1471,71, 357.25 [[1223] 354.26207 3.54.11" 3.64 0.04133 6.1172,-1471,71, 357.25 [[1223] 354.26207 3.54.11" 3.65 0.00213 7.171,-1471,71, 357.25 [[3353.255(8)	7.40×10^{5}	7.26	0.056(7)	$6d[7/2]_4 - 8p[5/2]_3$	3353.26 [L2228]
3373 387031 6.49 + 10° 6.19 0.001(0) 64(7), -17(7), 3383 73 (1228) 3384 385(14) 7.76 10° 5.25 0.008(13) 7.45(7), -5(17), 344 48 [12221] 3384 385(14) 7.76 10° 5.25 0.008(13) 7.45(7), -5(17), 344 48 [12221] 3384 385(14) 7.86 10 0.008(15) 7.45(7), -5(17), 344 48 [12221] 3497 730(7) 3.34 10° 6.23 0.008(15) 7.45(7), -47(7), 4 3532 365(2) 4.84 10° 10.2 0.007(3) 6.47(7), -47(7), 4 3353 12(20) 3533 1200 2.39 10° 6.59 0.003(3) 6.47(7), -47(7), 4 3563 12(22)] 3533 1200 2.39 10° 6.59 0.003(3) 647(7), -47(7), 4 3563 12(22)] 3533 1200 1.38 10° 6.66 0.033(2) 647(7), -47(7), 3 3563 12(22)] 3562 242(7) 10 1.38 10° 6.66 0.033(2) 647(7), -47(7), 3 3562 56 (1229)] 3562 42(7) 10 1.38 10° 5.78 10 0.005(2) 47(72), -67(7), 3 357(7) 11 [1249] 3562 42(7) 10 1.38 10° 3.66 <td>3365.674(16)</td> <td>8.37×10^{4}</td> <td>4.12</td> <td>0.057(14)</td> <td>$4f[9/2]_{5}-8d[7/2]_{4}$</td> <td></td>	3365.674(16)	8.37×10^{4}	4.12	0.057(14)	$4f[9/2]_{5}-8d[7/2]_{4}$	
383.723(19) 4/8 + 10 ⁶ 4.7 0.053(13) 7.15(1)-5(1)/2) 395.73 [1228] 384.224(0) 1.9 + 10 ⁶ 5.41 0.079(0) 7.15(1)-5(1)/2) 394.12 (1228) 382.246(2) 1.9 + 10 ⁶ 5.41 0.079(0) 7.15(1)-5(1)/2) 341.12 (1228) 382.246(2) 1.5 0.024(3) 7.15(1)-5(1)/2) 342.14 (1228) 300.235(3) 2.0 + 10 ⁻⁶ 6.0 0.031(3) 7.15(1)-5(1)/2) 355.75 (120) 325.575(3) 2.0 + 10 ⁻⁶ 6.0 0.031(3) 7.15(1)-5(1)/2) 355.75 (120) 355.575(3) 2.0 + 10 ⁻⁶ 6.0 0.031(3) 7.15(1)-5(1)/2) 355.75 (120) 355.575(3) 1.3 + 10 ⁻⁷ 5.3 0.096(9) 611/12)-5(1/2) 356.55 (1228) 355.575(3) 1.3 + 10 ⁻⁷ 6.40 0.051(4) 61/12)-5(1/2) 375.23 (1228) 375.377(1) 1.3 + 10 ⁻⁷ 6.40 0.051(4) 61/12)-5(1/2) 375.24 (1228) 375.377(1) 381.10 ⁻¹ 1.4 0.041(2) 61/12)-5(1/2) 375.27 (12) (1249) 385.767(2) 2.3 + 10 ⁻¹ 3.8 0.032(2) 41/72)-4(1/2) 385.77 (12) (1249) 385.775(1) 3.8 0.032(2) 41/72)-4(1/2) 385.77 (12) (1249) <td< td=""><td>3371.807(8)</td><td>6.89×10^{5}</td><td>6.19</td><td>0.061(6)</td><td>$6d[3/2]_1 - 5f[5/2]_2$</td><td>3371.81 [L2228]</td></td<>	3371.807(8)	6.89×10^{5}	6.19	0.061(6)	$6d[3/2]_1 - 5f[5/2]_2$	3371.81 [L2228]
3984.88(4) 70.0 16 ³ 5.26 0.081(3) 71/21, -51/21, 3042.84(7) 3042.84(2228) 3441.271(18) 2.0.0 197 71/21, -51/21, 3041.278 3042.84(2228) 3042.84(2228) 3441.271(18) 2.0.0 417 5.3.8 0.008(16) 71/31, -51/21, 3041.278 3041.278 320.0 560(10) 2.0.0 417 5.3.8 0.008(16) 71/31, -51/21, 41/31, -51/21, 3051.228 3050.10	3383.723(19)	4.68×10^{4}	4.57	0.045(18)	$7p[3/2]_1 - 7d[1/2]_1$	3383.73 [L2228]
shq2.2460) 1.9×10 ⁶ 5.4 0.07%0) 7.1/21, -41/21, 344.2.1 (1222) 3497.7537) 5.3 × 10 ⁶ 6.3 0.06813 7.1/21, -41/21, 344.7 (1223) 3497.7537) 5.3 × 10 ⁶ 1.0.2 0.00813 7.1/21, -41/21, 352.4 5 [1223] 352.451 5.0 × 10 ⁶¹ 1.0.2 0.007(3) 645.7 (-17), 352.4 5 [1223] 356.7 × 10.1 5.0 × 10 ⁶¹ 6.0 × 007(3) 647.7 (-17), -41/21, 352.4 5 [1223] 366.2 × 10 ⁶¹ 1.0 × 10 ⁶² 6.4 0.032(3) 641/21, -41/21, 366.5 0 [1223] 366.2 × 10 ⁶² 6.6 0.032(3) 641/21, -41/21, 366.2 5 [1223] 366.2 × 10 ⁶² 6.6 0.032(3) 641/21, -41/21, 366.2 5 [1223] 366.3 × 10 ⁶² 6.4 0.032(3) 641/21, -41/21, 366.2 5 [1223] 366.4 × 10 ⁶² 6.4 0.032(3) 641/21, -41/21, 366.2 5 [1223] 366.4 × 10 ⁶² 6.3 0.032(3) 41/121, -41/21, 365.6 [1223] 366.7 × 10 ⁶¹ 5.3 0.006(3) 7.1/12, -41/21,	3394.885(14)	7.70×10^{5}	5.25	0.085(13)	$7p[5/2]_2-5d'[5/2]_3$	3394.88 [L2228]
9447,97139) 2.9× 10 ² 5.38 0.083(16) 7.15/21,-171/21, 9447,97 (1228) 5520,353(0) 2.3 3 10 ⁻² 1.5 0.024(3) 7(1/21,-15/17/21, 3522,48 (1228) 5520,353(0) 2.3 3 10 ⁻² 1.6 0.024(3) 7(1/21,-15/17/21, 3522,48 (1228) 5520,353(0) 5.4 × 10 ⁻² 1.6 0.001(3) 7(1/21,-15/17/21, 3525,78 (1228) 5620,751(0) 5.0 × 10 ⁻² 6.4 0.001(3) 7(1/21,-15/17/21, 3565,78 (1228) 5662,721(6) 1.0 × 10 ⁻² 6.4 0.002(3) 6(1/21,-47(1/21,-14)) 3662,37 (1228) 5662,420(78) 3.1 × 10 ⁻² 6.40 0.005(4) 6(1/21,-47(1/21,-14)) 376,22 (1228) 5750,27(1) 3.9 × 10 ⁻² 6.40 0.005(4) 6(1/21,-47(1/21,-14)) 376,22 (1228) 5750,27(1) 3.9 × 10 ⁻² 5.8 0.005(5) 6(1/21,-47(1/21,-14)) 376,22 (1228) 586,420(78) 1.1 × 10 ⁻¹ 3.0 0.005(5) 7(1/21,-47(1/21,-14)) 387,178 (1228) 586,420(78) 1.1 × 10 ⁻¹ 3.0 0.005(3402.246(9)	1.39×10^{6}	5.41	0.079(6)	$7s[3/2]_1 - 7p[1/2]_0$	3402.24 [L2228]
3497.2302) 5.14 km ¹⁰ 6.23 0.068(5) ?1(2)_1-r(4)/2)_1 3497.23 (228) 352.456(2) 4.65 km ⁻¹ 1.62 0.037(3) 947/21-r(2)/2)_1 352.24 (228) 355.756(3) 5.0 x km ⁻¹ 6.6 0.037(3) 947/21-r(2)/2)_1 355.78 (1228) 355.756(3) 2.0 x km ⁻² 6.59 0.008(6) 941/21-r(2)/21, 355.78 (1228) 355.757(3) 2.0 x km ⁻² 6.59 0.008(2) 941/21-r(2)/21, 355.78 (1228) 355.247(3) 0.40 x m ⁻² 6.60 0.027(3) 941/21-r(2)/21, 375.83 (1228) 355.247(3) 0.40 x m ⁻² 6.60 0.023(3) 941/21-r(2)/21, 375.83 (1228) 355.798(2) 0.80 x m ⁻² 6.10 0.035(3) 71/21, -r(1)/21, 375.83 (1228) 357.247(2) 7.36 1.14 0.013(3) 71/21, -r(1)/21, 375.771.0 (1744) 358.597(2) 1.18 x m ⁻¹ 2.14 0.035(3) 71/21, -r(1)/21, 385.88 (1228) 357.795(2) 1.03 x m ⁻¹ 2.5 0.036(2) 71/21, -r(1)/21, 385.88 (1228) 357.795(2) 1.03 x m ⁻¹ 2.5 0.0	3441.791(18)	2.96×10^{5}	5.28	0.083(16)	$7p[3/2]_2 - 7d[1/2]_1$	3441.78 [L2228]
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3497.723(7)	5.34×10^{6}	6.23	0.068(5)	$7s[3/2]_2 - 7p[3/2]_2$	3497.73 [L2228]
3323.2800 4.3 k lp ⁻¹ 10.2 0.08700 ///1/1_2010/1 352.24 ft (228) 3553.75500 10.9 k lp ⁻¹ 6.59 0.030(0) 6/17/1_2-6/17/1 355.67 ft (228) 3553.75500 10.9 k lp ⁻¹ 6.59 0.030(0) 6/17/2-6/17/1 355.67 ft (228) 3553.75500 1.59 k lp ⁻¹ 2.41 0.060(27) 6/17/2-6/17/1 362.25 ft (228) 3662.257160 1.59 k lp ⁻¹ 6.66 0.031(3) 6/17/2-6/17/1 362.25 ft (228) 375.21700 6.89 k lp ⁻² 6.40 0.031(3) 6/17/2-6/17/1 375.32 ft (228) 375.21700 6.38 k lp ⁻¹ 6.10 0.037(2) 4/17/2-6/17/1 383.66 ft (222) 375.21700 2.38 k lp ⁻¹ 5.10 0.037(2) 4/17/2-6/17/1 383.66 ft (222) 385.69707 2.18 k lp ⁻¹ 5.10 0.037(2) 4/17/2-6/17/1 383.66 ft (228) 386.6977 2.18 k lp ⁻¹ 5.10 0.037(2) 4/17/2-6/17/1 397.78 ft (228) 397.15701 1.28 k lp ⁻¹ 5.10 0.037(2) 4/17/2-6/17/1	2520 252(4)	2.22×10^{-2}	11 5	0.024(2)	7-(1/2) 5-((2/2)	
bits bits <td>5520.353(4)</td> <td>2.33 × 10 -</td> <td>11.5</td> <td>0.024(3)</td> <td>$p_{1/2} - 3a' [5/2]_{2}$</td> <td>2533 45 [L 3338]</td>	5520.353(4)	2.33 × 10 -	11.5	0.024(3)	$p_{1/2} - 3a' [5/2]_{2}$	2533 45 [L 3338]
3233 1.20 1.29 0.00000 0.00000 0.00000 <td>0522.450(2)</td> <td>4.03×10^{-2}</td> <td>10.2</td> <td>0.037(3)</td> <td>$6p[3/2]_3 - 3a[3/2]_2$</td> <td>3522.45 [L2228]</td>	0522.450(2)	4.03×10^{-2}	10.2	0.037(3)	$6p[3/2]_3 - 3a[3/2]_2$	3522.45 [L2228]
323.1.600 2.0 0.000 0.071, -017, -	0000./00(0)	3.02×10^{-2}	10.0	0.031(3)	$s_{3/2} - p_{3/2}$	3555.78 [L2228]
9002-97010 1.0 9012	5559.182(0)	2.09×10^{-2}	0.39	0.030(6)	$6p[3/2]_2 - 7a[3/2]_2$	3559.17 [L2228]
982.14(2)/0) 1.9.8 0.9 1.9.8 0.001(4) 91(1/4)=91(1/1) 392.32 112.33 978.17(5) 6.60 0.005(3) 64(1/2)=41(72) 375.23 112.229] 978.17(5) 0.53 0.015(4) 64(1/2)=41(72) 375.23 112.229] 985.749(2) 7.56 1.34 0.025(5) 7.1(7)(2)=47(7) 385.65 376.23 112.229] 985.749(2) 7.56 1.01 10 ⁻¹ 3.66 0.025(5) 7.1(7)(1)=47(7) 385.747(2) 111 10.865.77(2) 1477(1)=46(77) 385.68 111 10.97 2.8 10.97 2.8 10.97 2.8 10.97 10.97 2.8 0.039(2) 7.1(7)=47(7) 387.78 10.97	0003.000(10)	2.31 × 10 -	5.55	0.060(9)	$6a[1/2]_1 - 8p[1/2]_1$	3003.30 [L2228]
abs. 2010 16 abs. 10 ⁻² 66 abs. 10 ⁻² abs. 10 ⁻² abs. 1122-31 3005.172 7.3 10.3 0.3 66 0.035(3) 66	0002.2/3(10)	1.50×10^{-2}	2.41	0.062(13)	$6a[1/2]_0 - 8p[1/2]_1$	3002.30 [L2228]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	002.402(78)	5.18×10^{-2}	6.00	0.032(78)	$6a[5/2]_2 - 8p[5/2]_2$	3002.30 [L2228]
74.303.20 9.36 0.88 0.0303 01/14]91/1, 25/14] 368.501(6) 841.2005) 1.13 × 10 ⁻¹ 3.66 0.035(2) 64/17/12]6(17)6(17) 368.501(2) 841.2016) 1.13 × 10 ⁻¹ 3.66 0.035(2) 47/17/12]6(17) 368.501(2) 866.2007) 2.18 × 10 ⁻¹ 5.78 0.044(6) 66/17/12]7(17) 387.173 [L223] 867.205(2) 1.07 × 10 ⁻¹ 2.81 0.039(2) 41/57.16(17) 387.173 [L223] 877.157(2) 1.07 × 10 ⁻¹ 2.6.5 0.039(2) 41/57.16(17) 387.173 [L223] 91.558(2) 1.35 × 10 ⁻¹ 2.4.6 0.039(2) 41/57.16(17) 993.36 [L2228] 91.558(2) 1.35 × 10 ⁻¹ 2.4.6 0.031(2) 41/92.16(17) 993.36 [L2228] 91.558(2) 1.3 × 10 ⁻¹ 2.6.7 0.031(2) 41/17.2]6(17.2] 993.36 [L2228] 91.558(2) 1.5 × 10 ⁻¹ 2.3 0.039(2) 41/52.16(17.2] 993.36 [L2228] 91.558(2) 7.5 × 10 ⁻² 6.61 0.072(13) 74/52 74/52 74/52 74/52	771 012(2)	6.80 × 10 -	6.40	0.031(4)	$6p[1/2]_0 - 3a[3/2]_1$	3/38.23 [L2228]
000.7.19/2 2.45 1.54 0.0413 067/12-31/21-4 380.57/12-11/21-4 884.50013 2.85 10 ⁻¹ 3.60 0.022(3) 241/71-4-67/121-4 380.566 11.2228 884.50013 1.15 10 ⁻¹ 3.60 0.022(3) 41/71-21-67/121-4 380.566 11.2228 884.50013 1.15 10 ⁻¹ 3.60 0.022(3) 41/71-21-67/121-4 380.566 11.2228 11.57	5//1.013(3)	9.47	6.60	0.035(3)	$6p[1/2]_0 - 5d[3/2]_1$	3//1.0/(11) [L/449]
8-3.690(2) 2.98 (0. 0.11) (0.12) 0.023(2) 417(7), -617(7), 438.686 (2223) 447(7), -617(7), -617(7), 438.686 (2223) 447(7), -617(7	0000.719(2)	7.30 2.20 · · 10= ²	13.4	0.041(3)	$6p[3/2]_2 - 5a[3/2]_2$	3805.77(12) [L/449]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	030.090(3) 941.790(5)	2.38 × 10 ~	0.10	0.020(3)	$s_{3}/2_{1}-0p'(1/2)_{1}$	3838.08 [L2228]
94.6.01(0) 1.01 × 10 ⁻¹ 3.60 0.394(2) 41/12/1; 37(3/1), 37(3) 971.755(6) 2.40 × 10 ⁻¹ 8.19 0.300(5) 71/12/2; -37(3/1), 71(3/2; -37(3/2), 41(3/2), -41(3/2), 41(3/2), -41(3/2), 41	041.720(5)	1.11 X 10 '	3.80	0.029(2)	$4J[7/2]_4 - 0g[9/2]_5$	
$\begin{aligned} \begin{array}{c} 8 = 0.8 = 37.7 \\ 2.48 \times 10^{-1} & 5.78 & 0.044(0) & 60[2/1]^{-1} \\ 872.157(2) & 1.07 \times 10^{-1} & 2.6.1 & 0.039(2) & 4f(72)_{-} 46[7(2)_{+} \\ 872.157(2) & 1.07 \times 10^{-1} & 2.6.1 & 0.039(2) & 4f(72)_{+} 46[7(2)_{+} \\ 883.31(2) & 9.61 \times 10^{-1} & 2.4.4 & 0.030(2) & 4f(72)_{-} 46[7(7)_{+} \\ 883.31(2) & 1.38 \times 10^{-1} & 2.4 & 0.030(2) & 4f(72)_{-} 46[17(1)_{+} \\ 992.158(2) & 1.38 \times 10^{-1} & 2.4 & 0.030(2) & 4f(72)_{-} 46[17(1)_{+} \\ 992.158(2) & 1.38 \times 10^{-1} & 2.4 & 0.030(2) & 4f(72)_{-} 46[17(1)_{+} \\ 992.158(2) & 1.38 \times 10^{-1} & 2.4 & 0.030(2) & 4f(72)_{-} 46[17(1)_{+} \\ 992.158(2) & 1.38 \times 10^{-1} & 2.4 & 0.030(2) & 4f(72)_{-} 46[17(1)_{+} \\ 993.1780(4) & 1.78 \times 10^{-1} & 2.4 & 0.030(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 993.987(7) & 7.78 \times 10^{-2} & 7.41 & 0.050(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 993.987(7) & 7.78 \times 10^{-2} & 8.64 & 0.035(5) & 7g[2/1]_{-} 74[7(1)_{+} \\ 993.989(3) & 3.99 \times 10^{-1} & 1.23 & 0.029(2) & 7g[2/1]_{-} 74[7(1)_{+} \\ 997.579(2) & 8.99 \times 10^{-1} & 1.23 & 0.029(2) & 7g[2/1]_{-} 74[7(1)_{+} \\ 997.579(2) & 8.99 \times 10^{-1} & 1.24 & 0.043(2) & 6g[2/1]_{-} 74[7(1)_{+} \\ 997.579(2) & 8.99 \times 10^{-1} & 1.26 & 0.038(3) & 7g[2/1]_{-} 74[7(1)_{+} \\ 997.579(2) & 2.67 \times 10^{-1} & 1.28 & 0.031(2) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.247(6) & 5.43 & 0.078(10) & 7g[1/1]_{-} 74[7(1)_{+} \\ 999.247(6) & 1.05 \times 10^{-1} & 1.26 & 0.038(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.942(7) & 1.05 \times 10^{-1} & 1.26 & 0.038(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.942(7) & 1.05 \times 10^{-1} & 1.26 & 0.038(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.942(7) & 1.05 \times 10^{-1} & 1.26 & 0.038(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.942(7) & 1.05 \times 10^{-1} & 1.26 & 0.038(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.942(7) & 1.05 \times 10^{-1} & 1.26 & 0.038(6) & 7g[2/1]_{-} 74[7(1)_{+} \\ 999.942(7) & 1.05 \times 10^{-1} & 0.08 \\ 0.117(7) & 0.05 \times 10^{-1} & 0.08 \\ 0.117(1) & 0.05 \times 10^{-1} & 0.07 \\ 0.117(1) & 0.05 \times 10^{-1} & 0.08 \\ 0.117(1) $	0041.001(0)	1.01 × 10 ⁻¹	3.20	0.030(2)	$4J[1/2]_3 - 0g[9/2]_4$	
$\begin{array}{c} 0.7.7.8.07 \\ 0.7.7.8.07 \\ 0.7.7.8.07 \\ 0.7.7.8.07 \\ 0.7.7.8.07 \\ 0.7.7.8.07 \\ 0.7.7.8.07 \\ 0$	000.89/(/)	2.18×10^{-2} 2.40 × 10^{-2}	5.78	0.044(6)	$5a[5/2]_3 - 5f[5/2]_3$	2071 70 11 22201
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	00/1./00(0)	2.40 × 10 ⁻²	8.19	0.030(5)	$p_{1}/2_{0} - a_{3}/2_{1}$	30/1./8 [L2228]
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	00/2.10/(2)	1.07×10^{-1}	28.1	0.029(2)	$4J[5/2]_2 - 6g[7/2]_3$	
3903.514/2 9.01 X 10 ⁻¹ 2.54 0.039(2) 61/2 9913.528(2) 1.3 X 10 ⁻¹ 2.7 0.031(2) 4/19/2,1-611/2,1/2,1 9913.58(2) 1.2 X 10 ⁻¹ 6.35 0.030(2) 4/13/2,1-615/2,1 9931.570(4) 5.7 X 10 ⁻² 9.80 0.035(3) 4/13/2,1-615/2,1 9931.570(7) 7.3 X 10 ⁻² 8.64 0.035(5) 74/3/2,1-7417/2,1 9973.57 (12.228) 9931.570(7) 7.3 X 10 ⁻² 8.61 0.072(13) 74/3/2,1-7417/2,1 9973.57 (12.228) 9973.579(12) 7.3 X 10 ⁻² 7.26 0.050(8) 74/3/2,1-7417/2,1 9975.70 (12.228) 9992.017(8) 3.0 X 10 ⁻² 7.26 0.050(8) 74/3/2,1-7417/2,1 4027.03(3) (17.449) 1005.090(3) 5.3 X 10 ⁻² 12.6 0.038(3) 74/3/2,1-7417/2,1 4027.03(3) (17.449) 1005.090(3) 5.3 X 10 ⁻¹ 12.8 0.038(3) 74/3/2,1-7417/2,1 4027.03(3) (17.449) 1005.090(3) 5.3 X 10 ⁻¹ 12.8 0.038(3) 74/3/2,1-7417/2,1 4027.03(3) (17.49) 1005.090(3) <td>00/0.125(2)</td> <td>1.07×10^{-1}</td> <td>26.5</td> <td>0.030(2)</td> <td>$4J[5/2]_3-6g[7/2]_4$</td> <td></td>	00/0.125(2)	1.07×10^{-1}	26.5	0.030(2)	$4J[5/2]_3-6g[7/2]_4$	
9):4.38(2) 1.31 × 10 ⁻¹ 24.7 0.031(2) 4/19/21,-611/21, 992.1.58(4) 1.22 × 10 ⁻¹ 6.35 0.030(2) 4/13/21,-615/21, 992.1.58(4) 5.7 × 10 ⁻² 9.80 0.055(3) 4/13/21,-615/21, 993.957(7) 7.7 × 10 ⁻² 7.41 0.050(6) 74/3/21,-7415/21, 993.36 [L2228] 996.918(6) 3.3 × 10 ⁻² 8.64 0.055(5) 74/3/21,-7415/21, 997.579(2) 8.9 × 10 ⁻¹ 1.2.3 0.029(2) 74/3/21,-7415/21, 997.579(2) 8.9 × 10 ⁻¹ 1.2.4 0.043(2) 66/3/21,-7415/21, 0025.093(3) 5.3 × 10 ⁻² 1.2.6 0.038(3) 74/3/2,-7415/21, 0027.147(2) 0.2.8 × 10 ² 0.039.24(4) 74/3/2,-7415/21, 0027.1671/21, 0.039.24(4) 74/3/2,-7415/21, 0.039.24(4) 74/3/2,-7415/21, 0.039.24(4) 74/3/2,-7415/21, 0.039.24(4) <td>3886.331(2)</td> <td>9.61×10^{-2}</td> <td>23.4</td> <td>0.030(2)</td> <td>$6d[5/2]_3 - 5f[7/2]_4$</td> <td></td>	3886.331(2)	9.61×10^{-2}	23.4	0.030(2)	$6d[5/2]_3 - 5f[7/2]_4$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3913.528(2)	1.33×10^{-1}	24.6	0.031(2)	$4f[9/2]_4-6g[11/2]_5$	
9922.154(3) 1.22 × 10 ⁻¹ 6.35 0.030(2) 4/1/32]-(qE/3/2). 9933.057(1) 7.73 × 10 ⁻² 9.80 0.035(3) 4/1/32]-(qE/3/2). 993.057(1) 7.73 × 10 ⁻² 8.64 0.035(5) 7/4/2)7/4(7/2). 999.051(6) 3.29 × 10 ⁻² 8.64 0.035(5) 7/4/2)7/4(7/2). 997.57(1).22281 999.21.750(1) 3.09 × 10 ⁻¹ 12.3 0.029(2) 7/6/3/2)7/4(7/2). 997.57(1).22281 997.57(10) 3.04 × 10 ⁻² 7.26 0.050(8) 7/6/3/2)7/4(7/2). 997.57(1).22281 997.57(1) 3.04 × 10 ⁻² 7.26 0.050(8) 7/6/3/2)7/4(7/2). 4027.03(13) [17.449] 902.017(8) 3.04 × 10 ⁻² 7.26 0.050(8) 7/6/3/2)6/4(7/2). 4027.03(13) [17.449] 903.05(0) 5.35 × 10 ⁻² 12.6 0.038(3) 7/6/3/2)6/4(7/2). 4027.03(13) [17.449] 903.05(0) 5.35 × 10 ⁻¹ 12.8 0.034(1) 7/6/3/26/4(7/2). 4027.03(13) [17.449] 903.920(1) 1.6 × 10 ¹⁰ 10.1 0.038(1) 7/6/2/26/12/2.1 4310.72(15) [17.449] 903.921(2) 1.6 × 10 ¹⁰ 10.8	3914.381(2)	1.58×10^{-1}	22.7	0.031(2)	$4f[9/2]_5-6g[11/2]_6$	
9931.570(4) 5.77 × 10 ⁻¹ 9.80 0.055(3) 47,1721,-747(2)], 9933.67(7) 77.3 × 10 ⁻¹ 7.41 0.050(6) 76,1721,-747(2)], 9939.86(7) 77.3 × 10 ⁻¹ 8.64 0.055(5) 76,1721,-747(2)], 9939.87(3) 7.30 × 10 ⁻² 8.61 0.072(13) 76,1721,-747(2)], 9973.579(13) 7.30 × 10 ⁻² 8.61 0.072(13) 76,1721,-67(172), 9973.579(13) 3.04 × 10 ⁻² 7.26 0.050(8) 76,1721,-747(2), 9992.017(8) 3.04 × 10 ⁻² 7.26 0.050(8) 76,1721,-747(2), 1025.039(3) 5.35 × 10 ⁻² 1.2.6 0.038(3) 76,1721,-747(2), 1025.039(3) 5.35 × 10 ⁻² 1.2.6 0.058(3) 76,1721,-747(2), 1025.039(3) 5.35 × 10 ⁻¹ 1.2.8 0.031(2) 76,1721,-747(2), 1025.039(3) 5.35 × 10 ⁻¹ 1.2.7 0.028(4) 71,1721,-747(2), 1025.039(3) 5.35 × 10 ⁻¹ 7.16 0.053(14) 66,1721,-747(2), 1029.939(5) 1.72 × 10 ⁴ 10.1 0.053(8) 76,1721,-747(2), 1029.939(5) 1.72 × 10 ⁴ 10.1 0.053(8) 76,1721,-747(2), 1029.939(5) 1.22 × 10 ⁵ 7.62 0.040(13) 67,1721,-747(2), 1029.939(5) 1.23 × 10 ⁵ 7.62 0.040(13) 67,1721,-747(2), 1029.9448(5) 1.72 × 10 ⁶ 6.484 0.061(6) 64,1721,-747(2), 1033.030(5) 4.22 × 10 ⁵ 6.484 0.061(6) 64,1721,-747(2), 1035.030(5) 1.22 × 10 ⁵ 7.54 0.057(7) 64,1721,-747(2), 1035.030(5) 1.22 × 10 ⁵ 7.54 0.057(7) 64,1721,-747(2), 1035.030(5) 1.22 × 10 ⁵ 7.54 0.057(7) 64,1721,-747(2), 1040.040(7) 7,16 × 10 ⁴ 7.54 0.057(7) 64,1721,-67(12), 1045.741(0) 40,721,-74(12), 1055.030(1) 4.33 × 10 ⁴ 3.34 0.044(20) 76,1721,-47(2), 1055.030(1) 4.33 × 10 ⁴ 3.34 0.044(20) 76,1721,-47(2), 1055.040(1) 4.05 × 10 ⁵ 7.54 0.057(7) 64,1721,-47(2), 1055.040(1) 4.05 × 10 ⁵ 7.54 0.057(7) 64,1721,-47(2), 1055.040(1) 4.05 × 10 ⁵ 7.54 0.057(7) 64,1721,-47(2), 1056.0306(8) 4.33 × 10 ⁴ 3.34 0.044(20) 76	3922.154(3)	1.22×10^{-1}	6.35	0.030(2)	$4f[3/2]_2-6g[5/2]_3$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3931.750(4)	5.77×10^{-2}	9.80	0.035(3)	$4f[3/2]_1 - 6g[5/2]_2$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3933.967(7)	7.73×10^{-2}	7.41	0.050(6)	$7p[3/2]_1 - 7d[5/2]_2$	3933.96 [L2228]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3959.631(6)	3.23×10^{-2}	8.64	0.035(5)	$7p[3/2]_2 - 7d[7/2]_3$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3969.489(8)	3.99×10^{-2}	11.1	0.056(8)	$7p[3/2]_1 - 7d[3/2]_1$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3973.579(13)	7.30×10^{-2}	8.61	0.072(13)	$7s[3/2]_2 - 6p'[3/2]_2$	3973.57 [L2228]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3975.719(2)	8.99×10^{-1}	12.3	0.029(2)	$7p[5/2]_3 - 7d[7/2]_4$	3975.70 [L2228]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3992.017(8)	3.04×10^{-2}	7.26	0.050(8)	$7p[3/2]_2 - 7d[5/2]_2$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4027.147(2)	4.27	12.4	0.043(2)	$6p[5/2]_3 - 5d[5/2]_3$	4027.03(13) [L7449]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4035.039(3)	5.35×10^{-2}	12.6	0.038(3)	$7p[3/2]_2 - 7d[3/2]_2$	
0409.932(4) 1.3×10^{-1} 12.7 0.028(4) $7_5[2]_2-67[1/2]_1$ 4177.554(7) 1.0×10^5 7.16 0.053(14) $6d[5/2]_2-7[1/2]_1$ 4177.554(7) 2.9×10^5 5.43 0.074(10) $7_{P[5/2]_1-74[1/2]_1}$ 4264.391(5) 2.71×10^5 10.1 0.053(8) $7_{P[5/2]_1-74[7/2]_1}$ 4294.448(5) 1.72×10^5 10.8 0.059(5) $7_{P[5/2]_1-74[7/2]_1}$ 4299.395(6) 1.29×10^5 5.24 0.070(6) $6p[5/2]_2-5d[5/2]_1$ 4310.72(15) [1.7449] 4332.403(7) 4.39×10^5 5.24 0.070(10) $7p[1/2]_1-74[1/2]_0$ 4342.416(7) 9.0×10^4 5.36 0.054(17) $6p[3/2]_2-5d[5/2]_1$ 4310.72(15) [1.7449] 4332.305(5) 4.22×10^5 6.64 0.060(7) $6p[3/2]_1-7d[3/2]_2$ 4359.456(3) 1.28×10^5 5.66 0.046(15) $5d[3/2]_1-6f[1/2]_1$ 4565.369(3) [1.9760] 4452.731(5) 4.20×10^5 5.62 0.057(7) $6p[1/2]_1-5d[3/2]_1$ 4565.369(3) [1.9760] 4457.510(6) 4.29×10^5 5.62 0.056(20) $7p[3/2]_1-5f[3/2]_1$ 4575.51(3) 4575.51(3)	4047.106(2)	2.67×10^{-1}	12.8	0.031(2)	$7p[3/2]_2 - 7d[5/2]_3$	
$\begin{array}{llllllllllllllllllllllllllllllllllll$	4089.932(4)	1.36×10^{-1}	12.7	0.028(4)	$7s[3/2]_2-6p'[1/2]_1$	
4201.157(7)2.96 10^3 5.430.074(10) $7p[1/2], -7d[7/2],$ 4264.391(5)2.71 $\times 10^3$ 10.10.053(8) $7p[5/2], -7d[5/2],$ 4294.48(5)1.72 $\times 10^6$ 10.80.059(5) $7p[5/2], -7d[5/2],$ 4299.395(6)1.29 $\times 10^5$ 7.620.040(13) $6p[5/2], -7d[5/2],$ 4310.411(5)3.80 $\times 10^3$ 5.240.070(6) $6p[5/2], -7d[5/2],$ 4322.803(7)4.39 $\times 10^5$ 5.240.070(6) $6p[5/2], -7d[5/2],$ 4324.416(7)9.09 $\times 10^4$ 5.360.054(17) $6p[13/2], -7d[3/2],$ 4353.305(5)4.22 $\times 10^5$ 6.840.061(6) $6d7[7], -57[9/2],$ 4460.04(7)7.16 $\times 10^5$ 5.180.82(7) $7d[3/2], -7d[5/2],$ 4460.704(7)1.00 $\times 10^6$ 6.400.104(20) $5d[3/2], -7d[5/2],$ 4465.781(5)4.26 $\times 10^5$ 7.040.060(7) $6d[7/2], -5f[9/2],$ 4465.781(5)9.41 $\times 10^6$ 7.450.05(7) $6p[1/2], -5d[5/2],$ 455.308(5)9.41 $\times 10^6$ 7.450.05(7) $6p[1/2], -5d[5/2],$ 467.513(7)9.83 $\times 10^5$ 5.820.105(9) $6p[3/2], -5d[5/2],$ 472.762(13)5.61 $\times 10^4$ 3.720.084(43) $6d[3/2], -6f[5/2],$ 472.752(13)5.61 $\times 10^4$ 3.720.084(43) $6d[3/2], -6f[5/2],$ 472.752(13)5.61 $\times 10^4$ 3.510.05(12) $7p[1/2], -7d[3/2],$ 473.520(11)2.57 $\times 10^4$ 6.530.050(12) $7p[1/2], -7d[3/2],$ 474.520(6)8.34 $\times 10^4$ 3.51<	4177.554(7)	1.05×10^{5}	7.16	0.053(14)	$6d[5/2]_2 - 7f[7/2]_3$	
4264 391(5)2.71 × 10 ⁵ 10.10.053(8) $7p[5/2]_{1}^{-7}d[5/2]_{2}^{-}$ 4294.448(5)1.72 × 10 ⁶ 10.80.059(5) $7p[5/2]_{2}^{-7}d[7/2]_{1}^{-}$ 4299.395(6)1.29 × 10 ⁵ 7.620.040(13) $6p[5/2]_{2}^{-7}d[7/2]_{1}^{-}$ 4310.411(5)3.80 × 10 ⁷ 8.470.070(6) $6p[5/2]_{2}^{-7}d[3/2]_{2}^{-}$ 4332.803(7)4.39 × 10 ³ 5.240.078(10) $7p[1/2]_{1}^{-7}d[1/2]_{2}$ 4342.416(7)909 × 10 ⁴ 5.360.054(17) $6p'(3/2]_{1}^{-7}d[3/2]_{2}^{-}$ 4353.305(5)4.22 × 10 ⁵ 6.840.061(6) $6q'(1/2]_{1}^{-5}p[9/2]_{4}^{-}$ 4369.858(5)1.28 × 10 ⁵ 7.550.060(10) $7p[5/2]_{2}^{-7d[3/2]_{2}^{-}}$ 4460.704(7)1.00 × 10 ⁶ 6.400.104(20)5d[3/2]_{1}^{-6}p[1/2]_{6}^{-}4465.781(5)4.26 × 10 ⁵ 7.040.000(7) $6q[1/2]_{4}^{-5}p[9/2]_{4}^{-}$ 4465.781(5)9.41 × 10 ⁶ 7.650.057(7) $6p[3/2]_{2}^{-5d[3/2]_{1}^{-}}$ 4465.781(5)9.41 × 10 ⁶ 7.450.057(7) $6p[3/2]_{2}^{-5d[3/2]_{1}^{-}}$ 4656.368(5)9.41 × 10 ⁶ 3.720.084(43) $6q[3/2]_{2}^{-5d[3/2]_{1}^{-}}$ 472.762(13)5.61 × 10 ⁴ 3.720.084(13) $6q[3/2]_{1}^{-6f[5/2]_{2}^{-}}$ 473.620(11)2.57 × 10 ⁴ 6.530.050(12) $7p[1/2]_{1}^{-7d[3/2]_{2}^{-}}$ 473.620(11)2.57 × 10 ⁴ 6.530.050(12) $7p[1/2]_{1}^{-7d[3/2]_{2}^{-}}$ 475.620(11)2.57 × 10 ⁴ 6.530.050(12) $7p[1/2]_{1}^{-7$	4201.157(7)	2.96×10^{5}	5.43	0.074(10)	$7p[1/2]_1 - 7d[1/2]_1$	
129 ± 10^6 10.80.059(5) $7p[5/2]_2 - 7d[7/2]_1$ $1299, 395(6)$ 1.29×10^5 7.620.040(13) $6p'[3/2]_1 - 7d[5/2]_2$ $130, 411(5)$ 3.80×10^7 8.470.070(6) $6p[5/2]_1 - 5d[5/2]_1$ $4310.72(15) [1.7449]$ $1332, 303(7)$ 4.39×10^5 5.240.078(10) $7p[1/2]_1 - 7d[1/2]_2$ $310.72(15) [1.7449]$ $1342, 416(7)$ 9.09×10^4 5.360.054(17) $6p'[3/2]_1 - 7d[3/2]_2$ $310.72(15) [1.7449]$ $1353, 305(5)$ 4.22×10^5 6.840.061(6) $6d[7/2]_1 - 5f(1/2]_1$ $410.72(17) [1.6]_1$ $335, 305(5)$ 1.28×10^5 7.550.060(10) $7p[5/2]_1 - 7d[3/2]_2$ $455.32(1) - 6p(1/2)_1$ $4461.704(7)$ 1.00×10^6 6.400.104(20) $5d[3/2]_1 - 6p(1/2)_1$ $477.51(5) - 25.50$ $4465.781(5)$ 4.26×10^5 7.04 0.060(7) $6d[1/2]_1 - 5d[5/2]_1$ $4655.369(3) [1.9760]$ $4455.781(5)$ 4.26×10^5 7.45 0.057(7) $6p[1/2]_1 - 5d[5/2]_1$ $4655.369(3) [1.9760]$ $4675.513(7)$ 9.85×10^5 5.82 0.105(9) $6p[3/2]_2 - 5d[3/2]_1$ $477.511(3) [1.9760]$ $472.762(13)$ 5.61×10^4 3.72 0.084(43) $6d[3/2]_1 - 6p[5/2]_2$ $479.412(3) [1.9760]$ $472.762(13)$ 5.61×10^4 3.72 0.084(43) $7p[1/2]_1 - 7d[5/2]_1$ $479.412(3) [1.9760]$ $475.502(11)$ 2.57×10^4 3.34 0.041(27) $7p[3/2]_1 - 9b[3/2]_1$ $479.412(3) [1.9760]$ $475.630(11)$ 5.72 0.084(43) <td< td=""><td>4264.391(5)</td><td>2.71×10^{5}</td><td>10.1</td><td>0.053(8)</td><td>$7p[5/2]_3 - 7d[5/2]_3$</td><td></td></td<>	4264.391(5)	2.71×10^{5}	10.1	0.053(8)	$7p[5/2]_3 - 7d[5/2]_3$	
	1294.448(5)	1.72×10^{6}	10.8	0.059(5)	$7p[5/2]_2 - 7d[7/2]_3$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4299.395(6)	1.29×10^{5}	7.62	0.040(13)	$6p'[3/2]_1 - 7d[5/2]_2$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4310.411(5)	3.80×10^{7}	8.47	0.070(6)	$6p[5/2]_2 - 5d[5/2]_3$	4310.72(15) [L7449]
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4332.803(7)	4.39×10^{5}	5.24	0.078(10)	$7p[1/2]_1 - 7d[1/2]_0$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4342.416(7)	9.09×10^{4}	5.36	0.054(17)	$6p'[3/2]_1 - 7d[3/2]_2$	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4353.305(5)	4.22×10^{5}	6.84	0.061(6)	$6d[7/2]_2 - 5f[9/2]_4$	
H420.004(7)7.16 × 10 ⁵ 5.180.082(7)7.3(3/2)_1-6f(1/2)_0H461.704(7)1.00 × 10 ⁶ 6.400.104(20)5d(3/2)_1-7p(5/2)_2H465.781(5)4.26 × 10 ⁵ 7.040.060(7)6d(1/2)_4-5f(9/2)_3H489.155(6)1.22 × 10 ⁵ 5.060.046(15)5d(3/2)_1-6f(3/2)_1H656.368(5)9.41 × 10 ⁶ 7.450.057(7)6p(1/2)_1-5d(5/2)_2H657.513(7)9.85 × 10 ⁵ 5.820.105(9)6p(3/2)_2-5d(3/2)_1H693.006(8)4.93 × 10 ⁴ 3.880.045(24)6d(3/2)_2-5f(5/2)_3H711.752(8)4.08 × 10 ⁴ 4.750.036(20)7p(3/2)_2-9s(3/2)_1H727.762(13)5.61 × 10 ⁴ 3.720.084(43)6d(3/2)_1-6f(5/2)_2H735.620(11)2.57 × 10 ⁴ 3.340.041(27)7p(3/2)_2-9s(3/2)_1H751.401(6)8.79 × 10 ⁴ 6.530.050(12)7p(1/2)_1-7d(3/2)_1H796.590(8)4.02 × 10 ⁴ 4.840.044(24)7p(1/2)_1-7d(3/2)_1H794.401(7)1.16 × 10 ⁵ 5.720.048(15)7p(1/2)_1-7d(3/2)_2H794.401(7)1.16 × 10 ⁵ 6.660.011(18)	1369.858(5)	1.28×10^{5}	7.55	0.060(10)	$7p[5/2]_{2}-7d[3/2]_{2}$	
4461.704(7) 1.00×10^6 6.40 $0.104(20)$ $5d[3/2]_1 - 7p[5/2]_2$ 4465.781(5) 4.26×10^5 7.04 $0.060(7)$ $6d[7/2]_1 - 5p[9/2]_3$ 4489.155(6) 1.22×10^5 5.06 $0.046(15)$ $5d[3/2]_1 - 6p[3/2]_1$ 4656.368(5) 9.41×10^6 7.45 $0.057(7)$ $6p[1/2]_1 - 5d[5/2]_2$ $4656.369(3)$ $1667.513(7)$ 9.85×10^5 5.82 $0.105(9)$ $6p[3/2]_2 - 5d[3/2]_1$ $4677.511(3)$ $1693.006(8)$ 4.93×10^4 3.88 $0.045(24)$ $6d[3/2]_1 - 6f[5/2]_3$ $1727.762(13)$ 5.61×10^4 3.72 $0.084(43)$ $6d[3/2]_1 - 6f[5/2]_2$ $1727.762(13)$ 5.61×10^4 3.72 $0.084(43)$ $6d[3/2]_1 - 6f[5/2]_2$ $1727.762(13)$ 5.61×10^4 3.72 $0.084(43)$ $6d[3/2]_1 - fd[5/2]_2$ $1727.62(13)$ 5.61×10^4 3.34 $0.041(27)$ $7p[3/2]_2 - 9s[3/2]_1$ $1751.401(6)$ 8.79×10^4 6.53 $0.050(12)$ $7p[1/2]_1 -7d[5/2]_2$ $1786.940(8)$ 4.02×10^4 4.84 $0.044(24)$ $7p[1/2]_1 -7d[5/2]_2$ $1784.401(7)$ 1.16×10^5 5.72 $0.048(15)$ $7p[1/2]_1 -7d[3/2]_1$ $1794.401(7)$ 1.61×10^5 5.72 $0.048(15)$ $7p[1/2]_1 -7p[3/2]_2$ $4794.529(3)$ $1794.401(7)$ 1.61×10^5 5.72 $0.048(15)$ $7p[1/2]_1 -7p[3/2]_2$ $4794.529(3)$ $1794.401(7)$ 1.61×10^5 5.72 $0.048(15)$ $7p[1/2]_1 -7p[3/2]_2$ $4794.529(3)$ $1794.401(7)$	1420.004(7)	7.16×10^{5}	5.18	0.082(7)	$7s[3/2]_1 - 6p'[1/2]_0$	
4465.781(5) 4.26×10^3 7.04 $0.60(7)$ $60(7/2)_{14} - 51/9/2)_{5}$ 4489.155(6) 1.22×10^5 5.06 $0.046(15)$ $5d[3/2)_1 - 6p'[3/2)_1$ 4656.368(5) 9.41×10^6 7.45 $0.057(7)$ $6p[1/2)_1 - 5d[5/2)_2$ $4656.369(3)$ 4677.513(7) 9.85×10^5 5.82 $0.105(9)$ $6p[3/2)_2 - 5d[3/2)_1$ $4677.511(3)$ $1693.006(8)$ 4.93×10^4 3.88 $0.045(24)$ $6d[3/2)_2 - 5f[5/2)_3$ $477.512(3)$ $4711.752(8)$ 4.08×10^4 4.75 $0.036(20)$ $7p[3/2)_2 - 9s[3/2]_2$ $4785.620(11)$ 2.57×10^4 3.72 $0.084(43)$ $6d[3/2)_1 - 6f[5/2)_2$ $4786.940(8)$ 4.02×10^4 4.84 $0.044(27)$ $7p[3/2)_2 - 9s[3/2]_1$ $4794.412(3)$ $4794.401(7)$ 1.16×10^5 5.72 $0.048(15)$ $7p[1/2)_1 - 7d[3/2]_1$ $4794.412(3)$ $4794.401(7)$ 1.16×10^5 5.72 $0.048(15)$ $7p[1/2)_1 - 7d[3/2]_2$ $4794.529(3)$ $4796.529(3)$ 1.90×10^5 5.46 $0.111(18)$ $5d[3/2)_1 - 7p[3/2]_2$ $4794.529(3)$ $4920.027(5)$ 1.24×10^5 9.90 $0.038(9)$ $7p[5/2]_3 - 8s[3/2]_2$ $4920.029(3)$ $4920.029(3)$ 1.97601 $5224.92(10)$ 4.00×10^{-2} 4.73 $0.016(6)$ $5d[3/2]_1 - 7p[3/2]_2$ $4920.029(3)$ $4920.029(5)$ 1.24×10^5 9.90 $0.038(9)$ $7p[5/2]_3 - 8s[3/2]_1$ $493.941(3)$ 1.97601 $4922.029(5)$ 1.24×10^5 6.66 $0.064(6)$ 5	4461.704(7)	1.00×10^{6}	6.40	0.104(20)	$5d[3/2]_1 - 7p[5/2]_2$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4465.781(5)	4.26×10^{5}	7.04	0.060(7)	$6d[7/2]_4 - 5f[9/2]_5$	
4656.368(5)9.41 × 10 ⁶ 7.450.057(7)6p[1/2]_1-5d[5/2]_24656.369(3) [L9760]4677.513(7)9.85 × 10 ⁵ 5.820.105(9) $6p[3/2]_2-5d[3/2]_1$ 4677.511(3) [L9760]4693.006(8)4.93 × 10 ⁴ 3.880.045(24) $6d[3/2]_2-5f[5/2]_3$ 4677.511(3) [L9760]4711.752(8)4.08 × 10 ⁴ 4.750.036(20) $7p[3/2]_2-9s[3/2]_2$ 4778.752(13)5.61 × 10 ⁴ 3.720.084(43) $6d[3/2]_1-6f[5/2]_2$ 4735.620(11)2.57 × 10 ⁴ 3.340.041(27) $7p[3/2]_2-9s[3/2]_1$ 4794.401(7)4794.401(7) $7p[1/2]_1-7d[5/2]_2$ 4786.940(8)4.02 × 10 ⁴ 4.840.044(24) $7p[1/2]_1-7d[3/2]_2$ 4794.412(3) [L9760]4794.401(7)1.16 × 10 ⁵ 5.720.048(15) $7p[1/2]_1-7d[3/2]_2$ 4794.412(3) [L9760]4796.535(7)1.90 × 10 ⁵ 5.460.111(18) $5d[3/2]_1-7p[3/2]_1$ 4854.583(3) [L9760]4854.596(8)8.34 × 10 ⁴ 3.510.061(25) $5d[3/2]_1-7p[3/2]_1$ 4854.583(3) [L9760]4929.037(5)1.24 × 10 ⁵ 9.900.038(9) $7p[5/2]_3-9s[3/2]_2$ 4929.029(3) [L9760]4933.945(6)3.12 × 10 ⁷ 6.770.091(4) $6p[3/2]_1-5d[3/2]_1$ 4933.941(3) [L9760]4952.284(5)8.94 × 10 ⁵ 6.660.064(6) $5d[3/2]_1-7p[1/2]_4$ 4952.282(3) [L9760]5234.924(12)1.01 × 10 ⁻³ 3.970.115(25) $6d[5/2]_3-6f[7/2]_4$ 5321.052(3) [L9760]5471.083(13)8.53 × 10 ⁻⁴ 3.950.093(41) $7p[1/2]_1-9s[3/2]_2$ 5471.	4489.155(6)	1.22×10^{5}	5.06	0.046(15)	$5d[3/2]_1 - 6p'[3/2]_1$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4656.368(5)	9.41×10^{6}	7.45	0.057(7)	$6p[1/2]_1 - 5d[5/2]_2$	4656.369(3) [1.9760]
4693.006(8)4.93 × 1043.880.045(24) $6d[3/2]_2-5f[5/2]_3$ 4711.752(8)4.08 × 1044.750.036(20) $7p[3/2]_2-9s[3/2]_2$ 4727.762(13)5.61 × 1043.720.084(43) $6d[3/2]_1-6f[5/2]_2$ 4735.620(11)2.57 × 1043.340.041(27) $7p[3/2]_2-9s[3/2]_1$ 4751.401(6)8.79 × 1046.530.050(12) $7p[1/2]_1-7d[5/2]_2$ 4786.940(8)4.02 × 1044.840.044(24) $7p[1/2]_1-7d[3/2]_1$ 4794.401(7)1.16 × 1055.720.048(15) $7p[1/2]_1-7d[3/2]_2$ 4796.535(7)1.90 × 1055.460.111(18) $5d[3/2]_1-7p[3/2]_2$ 4796.535(7)1.90 × 1055.460.111(18) $5d[3/2]_1-7p[3/2]_2$ 4854.596(8)8.34 × 1043.510.061(25) $5d[3/2]_1-7p[3/2]_2$ 4929.029(3) [L9760]4933.945(6)3.12 × 1076.770.091(4) $6p[3/2]_1-5p[3/2]_1$ 4952.284(5)8.94 × 1056.660.064(6) $5d[3/2]_1-7p[1/2]_0$ 4952.284(5)8.94 × 1056.660.064(6) $5d[3/2]_1-7p[1/2]_0$ 5234.924(12)1.01 × 10^{-3}3.970.115(25) $6d[5/2]_2-6f[7/2]_4$ 5471.083(13)8.53 × 10^{-4}3.950.093(41) $7p[1/2]_1-s[3/2]_2$ 5471.097(3) [L9760]5526.222(2)8.78 × 10^{-4}2.320.143(57) $6d[5/2]_2-6f[7/2]_3$	4677.513(7)	9.85×10^{5}	5.82	0.105(9)	$6p[3/2]_2 - 5d[3/2]_1$	4677.511(3) [L9760]
1711.752(8)4.08 × 10 ⁴ 4.750.036(20) $7p[3/2]_2-9s[3/2]_2$ 4727.762(13)5.61 × 10 ⁴ 3.720.084(43) $6d[3/2]_1-6f[5/2]_2$ 4735.620(11)2.57 × 10 ⁴ 3.340.041(27) $7p[3/2]_2-9s[3/2]_1$ 4751.401(6)8.79 × 10 ⁴ 6.530.050(12) $7p[1/2]_1-7d[5/2]_2$ 4786.940(8)4.02 × 10 ⁴ 4.840.044(24) $7p[1/2]_1-7d[3/2]_1$ 4794.401(7)1.16 × 10 ⁵ 5.720.048(15) $7p[1/2]_1-7d[3/2]_2$ 4796.535(7)1.90 × 10 ⁵ 5.460.111(18) $5d[3/2]_1-7p[3/2]_2$ 4796.535(7)1.90 × 10 ⁵ 5.460.111(18) $5d[3/2]_1-7p[3/2]_2$ 4929.037(5)1.24 × 10 ⁵ 9.900.038(9) $7p[5/2]_3-9s[3/2]_2$ 4929.029(3)1.9760]4933.945(6)3.12 × 10 ⁷ 6.770.091(4) $6p[3/2]_1-5d[3/2]_1$ 4952.284(5)8.94 × 10 ⁵ 6.660.064(6) $5d[3/2]_1-7p[1/2]_4$ 5234.924(12)1.01 × 10 ⁻³ 3.970.115(25) $6d[5/2]_2-6f[7/2]_4$ 5234.924(12)1.01 × 10 ⁻³ 3.970.116(13) $6p[1/2]_0-rs[3/2]_1$ 5321.052(3) [L9760]5471.083(13)8.53 × 10 ⁻⁴ 3.950.093(41) $7p[1/2]_0-s[3/2]_2$ 5471.097(3) [L9760]5526.222(21)8.78 × 10 ⁻⁴ 2.320.143(57) $6d[5/2]_2-6f[7/2]_3$	4693.006(8)	4.93×10^{4}	3.88	0.045(24)	$6d[3/2]_{2} - 5f[5/2]_{2}$	
4727.762(13)5.61 × 10 ⁴ 3.720.084(43) $6d[3/2]_1-6f[5/2]_2$ 4735.620(11)2.57 × 10 ⁴ 3.340.041(27) $7p[3/2]_2-9s[3/2]_1$ 4751.401(6)8.79 × 10 ⁴ 6.530.050(12) $7p[1/2]_1-7d[5/2]_2$ 4786.940(8)4.02 × 10 ⁴ 4.840.044(24) $7p[1/2]_1-7d[3/2]_1$ 4794.401(7)1.16 × 10 ⁵ 5.720.048(15) $7p[1/2]_1-7d[3/2]_2$ 4796.535(7)1.90 × 10 ⁵ 5.460.111(18) $5d[3/2]_1-7p[3/2]_2$ 4854.596(8)8.34 × 10 ⁴ 3.510.061(25) $5d[3/2]_1-7p[3/2]_1$ 4854.596(3)1.24 × 10 ⁵ 9.900.038(9) $7p[5/2]_3-9s[3/2]_1$ 4929.037(5)1.24 × 10 ⁵ 9.900.038(9) $7p[5/2]_3-9s[3/2]_1$ 4933.945(6)3.12 × 10 ⁷ 6.770.091(4) $6p[3/2]_1-5d[3/2]_1$ 4935.284(5)8.94 × 10 ⁵ 6.660.064(6) $5d[3/2]_1-7p[1/2]_0$ 5234.924(12)1.01 × 10 ⁻³ 3.970.115(25) $6d[5/2]_3-6f[7/2]_4$ 5321.046(10)4.00 × 10 ⁻² 4.730.116(13) $6p[1/2]_0-7s[3/2]_1$ 5471.083(13)8.53 × 10 ⁻⁴ 3.950.093(41) $7p[1/2]_1-9s[3/2]_2$ 5526.222(21)8.78 × 10 ⁻⁴ 2.320.143(57) $6d[5/2]_2-6f[7/2]_3$	4711.752(8)	4.08×10^{4}	4.75	0.036(20)	$7p[3/2]_2 - 9s[3/2]_2$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4727.762(13)	5.61×10^{4}	3.72	0.084(43)	$6d[3/2]_{1} - 6f[5/2]_{2}$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4735.620(11)	2.57×10^{4}	3.34	0.041(27)	$7p[3/2]_2 - 9s[3/2]_2$	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4751.401(6)	8.79×10^4	6 53	0.050(12)	$7p[1/2]_{2} = 7d[5/2]_{1}$	
1100000000000000000000000000000000000	4786.940(8)	4.02×10^4	4 84	0.044(24)	7n[1/2], -7d[3/2].	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4794.401(7)	1.16×10^5	5 72	0.048(15)	7n[1/2] = 7d[3/2]	4794 412(3) [1.9760]
$\begin{array}{c ccccc} & 1.10 \times 10^{-1} & 5.10 & 0.111(10) & 54(1/2)_1^{-1}p_1/2)_{12} & 4790.329(3) \\ 4854.596(8) & 8.34 \times 10^4 & 3.51 & 0.061(25) & 54(3/2)_1^{-1}p_1/3/2)_1 & 4854.583(3) [L9760] \\ 4929.037(5) & 1.24 \times 10^5 & 9.90 & 0.038(9) & 7p[5/2]_3 - 9s[3/2]_2 & 4929.029(3) [L9760] \\ 4933.945(6) & 3.12 \times 10^7 & 6.77 & 0.091(4) & 6p[3/2]_1 - 54(3/2)_1 & 4933.941(3) [L9760] \\ 4952.284(5) & 8.94 \times 10^5 & 6.66 & 0.064(6) & 5d(3/2)_1 - 7p[1/2]_0 & 4952.282(3) [L9760] \\ \hline 5234.924(12) & 1.01 \times 10^{-3} & 3.97 & 0.115(25) & 6d(5/2)_3 - 6f(7/2)_4 \\ \hline 5234.924(12) & 4.00 \times 10^{-2} & 4.73 & 0.116(13) & 6p[1/2]_0 - 7s[3/2]_1 & 5321.052(3) [L9760] \\ \hline 5471.083(13) & 8.53 \times 10^{-4} & 3.95 & 0.093(41) & 7p[1/2]_1 - 9s[3/2]_2 & 5471.097(3) [L9760] \\ \hline 5526.222(21) & 8.78 \times 10^{-4} & 2.32 & 0.143(57) & 6d[5/2]_2 - 6f[7/2]_3 \end{array}$	4796 535(7)	1.10×10^{5}	5 46	0.111(18)	$5d[3/2] = 7n[3/2]_2$	4796 529(3) [19760]
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1854 596(8)	1.70×10 8 34 × 10 ⁴	3.50	0.061(25)	$5a[3/2]_1 - p[5/2]_2$ $5d[3/2]_2 - 7p[3/2]_2$	4854 583(3) [L9/00]
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4020 037(5)	1.24×10^5	0.01	0.001(23)	$3u[3/2]_1 - p[3/2]_1$ 7n[5/2] = 0n[2/2]	4020 (22012) [10740]
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1033 045(6)	1.24×10^{-107}	9.90 6 77	0.030(9)	$p_{[3/2]_3} - y_{[3/2]_2}$	4022 041(2) [L3/00]
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1052 284(5)	3.12×10^{-105}	0.//	0.091(4)	5d[2/2] = 5u[5/2]	4050 202(2) [L9/00]
	1732.204(3)	0.94 X 10°	0.00	0.004(0)	$3u_{1}3/2J_{1}-p_{1}2J_{0}$	4932.262(3) [L9/60]
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5234.924(12)	1.01×10^{-3}	3.97	0.115(25)	$6d[5/2]_3 - 6f[7/2]_4$	
$5471.083(13)$ 8.53×10^{-4} 3.95 $0.093(41)$ $7p[1/2]_1 - 9s[3/2]_2$ $5471.097(3)$ [L9760] $5526.222(21)$ 8.78×10^{-4} 2.32 $0.143(57)$ $6d[5/2]_2 - 6f[7/2]_3$	5321.046(10)	4.00×10^{-2}	4.73	0.116(13)	$6p[1/2]_0 - 7s[3/2]_1$	5321.052(3) [L9760]
5526.222(21) 8.78 × 10 ⁻⁴ 2.32 0.143(57) $6d[5/2]_2 - 6f[7/2]_3$	5471.083(13)	8.53×10^{-4}	3.95	0.093(41)	$7p[1/2]_1 - 9s[3/2]_2$	5471.097(3) [L9760]
	5526.222(21)	8.78×10^{-4}	2.32	0.143(57)	$6d[5/2]_2 - 6f[7/2]_3$	

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Table 2 (continued).

v_{ki} (cm ⁻¹)	I _{ki}	SNR	FWHM	Identification	Other work
	(arb. u.)		(cm ⁻¹)		(if any)
5683.494(11)	1.98×10^{-3}	4.40	0.122(15)	$7p[3/2]_2 - 8d[5/2]_3$	
5718.328(13)	3.04×10^{-3}	4.01	0.127(21)	$7s[3/2]_2 - 4f[5/2]_3$	5718.290(3) [L9760]
5719.819(18)	5.37×10^{-4}	2.30	0.088(65)	$6d[7/2]_3-6f[9/2]_4$	
5757.103(17)	4.81×10^{-3}	2.82	0.113(21)	$7p[5/2]_3 - 8d[7/2]_4$	5757.099(3) [L9760]
5770.171(23)	2.30×10^{-1}	2.29	0.164(18)	$6p[5/2]_2 - 5d[3/2]_1$	5770.164(3) [L9760]
5921.449(17)	2.47×10^{-3}	2.84	0.122(22)	$5d[5/2]_3 - 7p[5/2]_2$	5921.473(3) [L9760]
5938.536(15)	2.72×10^{-3}	2.96	0.107(27)	$p_{5/2_{2}} - 8d_{7/2_{3}}$	E070 044(2) [10760]
5970.042(16)	4.31×10^{-1}	2.82	0.111(20)	$5a[5/2]_1 - 6p[1/2]_0$ $6p[3/2]_1 - 7p[3/2]_0$	5970.044(3) [L9700] 5076 312(3) [L9760]
6039 003(17)	1.08×10^{-2}	2.03	0.123(18)	$5d[5/2]_2 - 7s[5/2]_2$	6039 1 [L2228]
6227.548(10)	1.07×10^{-1}	4.86	0.108(13)	$6p[3/2]_{2}-7s[3/2]_{1}$	6228.04(4) [L7384]
6232.739(10)	7.11×10^{-3}	4.88	0.110(14)	$6p[3/2]_1 - 7s[3/2]_2$	6232.7 [L2228]
6256.296(9)	2.65×10^{-2}	4.99	0.104(14)	$5d[5/2]_3 - 7p[3/2]_2$	6256.3 [L2228]
6300.867(15)	1.25×10^{-3}	3.45	0.133(47)	$7p[1/2]_1 - 8d[1/2]_1$	6300.9 [L2228]
6358.535(18)	1.19×10^{-3}	2.69	0.120(34)	$7p[1/2]_1 - 8d[3/2]_2$	6358.5 [L2228]
6426.163(7)	1.14×10^{-2}	8.01	0.107(11)	$5d[5/2]_2 - 7p[5/2]_2$	6426.2 [L2228]
6442.252(16) 6452.600(18)	1.38×10^{-3}	2.88	0.117(26)	$6p'[1/2]_1 - (s'[1/2]_0)$	6442.2 [L2228]
6483 980(10)	2.57×10^{-1}	2.80 4.86	0.141(24) 0.113(12)	$5a[5/2]_2 = 6p[5/2]_1$ $6p[3/2]_2 = 7s[3/2]_1$	0433.0 [L2228]
6620 809(11)	6.92×10^{-3}	4.62	0.118(16)	$6p[1/2]_1 - 5d[3/2]_1$	6620 8 [L2228]
6638.219(10)	2.26×10^{-3}	4.84	0.100(19)	$6p'[3/2]_2 - 7s'[1/2]_1$	6638.2 [L2228]
6732.171(9)	1.27×10^{-3}	5.94	0.118(22)	$5d[5/2]_3-6p'[3/2]_2$	6732.2 [L2228]
6780.727(16)	1.13×10^{-3}	2.72	0.100(44)	$7p[5/2]_3 - 9d[7/2]_4$	
6785.712(10)	5.99×10^{-1}	4.61	0.111(13)	$6p[5/2]_3 - 7s[3/2]_2$	
6819.040(11)	1.10×10^{-2}	4.34	0.116(16)	$5d[5/2]_2 - 7p[3/2]_1$	6819.49(4) [L7384]
6893.070(17)	1.44×10^{-3}	2.69	0.111(41)	$[s_{3/2}]_{1} = 8p[3/2]_{1}$	6893.0 [L2228]
6930.930(17) 6040.801(10)	1.00×10^{-3}	2.82	0.120(34)	$s_{12}/2_{1}-8p_{1}/2_{2}$	6930.9 [L2228]
6949.801(10) 6959.464(9)	1.85×10^{-2}	4.95 5.28	0.110(18)	$5a[5/2]_1 - 4f[5/2]_1$ 5d[3/2] 4f[3/2]	6949.9(2) [L4085] 6959 51(4) [I 7384]
6964 499(22)	1.89×10^{-3}	2.33	0.160(29)	$5u[5/2]_1 \rightarrow f[5/2]_2$ $7s[3/2]_2 - 8v[1/2]_2$	6964 5 [L4211c2]
7020.076(11)	6.67×10^{-2}	4.40	0.112(14)	$5d[3/2]_2 = 4f[5/2]_2$	7019.87(4) [L7384]
7032.596(17)	5.97×10^{-4}	2.77	0.108(45)	$7s[3/2]_2 - 8p[5/2]_2$	7032.6 [L2228]
7068.974(15)	1.29×10^{-1}	3.10	0.119(14)	$6p[5/2]_2 - 7s[3/2]_2$	
7076.169(15)	4.10×10^{-3}	3.00	0.111(17)	$7s[3/2]_2 - 8p[5/2]_3$	7076.2 [L2228]
7115.084(17)	1.11×10^{-3}	2.69	0.106(45)	$7s[3/2]_1 - 8p[1/2]_0$	7115.1 [L2228]
7320.216(14)	2.71×10^{-1}	3.32	0.116(14)	$6p[5/2]_2 - 7s[3/2]_1$	F001 040 [7 0000]
7381.240(15)	2.49×10^{-2} 3.04×10^{-3}	3.17	0.113(17)	$5d[7/2]_3 - 7p[5/2]_2$ $5d[7/2]_3 - 7p[5/2]_2$	7381.242 [L2228]
7498.707(10)	5.52 10-5	4.78	0.101(18)	5u[//2] ₃ =/p[5/2] ₃	7450.0 [L2220]
8050.377(5)	5.53×10^{-3}	10.1	0.032(5)	$5d[3/2]_2 - 6p[3/2]_1$	8056.4 [L2228] 8155 822(20) [17202]
8170 870(5)	1.74×10^{-2}	23.5	0.042(3)	$5u[1/2]_0 - 7p[1/2]_1$ $6v[1/2]_0 - 7s[3/2]_1$	8170 877(20) [L7293]
8191.910(15)	4.29×10^{-4}	6.29	0.060(14)	$5d[7/2]_3-6p'[3/2]_2$	8192.1(2) [L4085]
8272.585(5)	4.51×10^{-3}	13.3	0.038(3)	$5d[7/2]_4 - 7p[5/2]_3$	8272.594(21) [L7293]
8363.754(5)	2.88×10^{-3}	37.8	0.054(3)	$5d[3/2]_2 - 7p[3/2]_2$	8363.812(21) [L7293]
8365.065(8)	3.27×10^{-4}	9.26	0.038(7)	$5d[1/2]_1 - 7p[5/2]_2$	8365.14(7) [L7293]
8392.509(6)	1.06×10^{-3}	18.5	0.046(4)	$5d[1/2]_1 - 6p'[3/2]_1$	8392.528(21) [L7293]
8419.243(16)	3.49×10^{-3}	5.53	0.052(14)	$5a[5/2]_3 - 4f[3/2]_2$	8419.202(21) [L/293] 8420.017(21) [L7202]
8431 302(7)	2.20×10^{-3}	18.0 5.72	0.030(3)	$5/[1/2]_0 - 0a[1/2]_1$	8431 308(21) [L7293]
8476.895(8)	6.07×10^{-3}	14.8	0.052(6)	$5d[5/2]_3 = 4f[5/2]_2$	8476.884(22) [L7293]
8513.926(5)	2.87×10^{-2}	18.9	0.039(2)	$5d[5/2]_3 - 4f[7/2]_4$	8513.935(6) [L9760]
8607.857(8)	3.55×10^{-3}	13.1	0.065(6)	$5d[1/2]_0 - 6p'[3/2]_1$	8607.882(22) [L7293]
8699.883(5)	1.48×10^{-3}	23.4	0.044(3)	$5d[1/2]_1 - 7p[3/2]_2$	8699.914(23) [L7293]
8757.944(6)	1.24×10^{-3}	19.3	0.043(3)	$5d[1/2]_1 - 7p[3/2]_1$	8757.974(23) [L7293]
8855.646(8)	7.24×10^{-4}	11.9	0.060(7)	$5d[1/2]_1 - 7p[1/2]_0$	8855.677(24) [L7293]
8973.292(7)	1.84×10^{-3}	15.2	0.075(5)	$5d[1/2]_0 - p[3/2]_1$	8973.281(3) [L9760]
9018 541(5)	4.19×10^{-2}	16.5	0.038(3)	$5d[5/2]_2 \rightarrow f[5/2]_2$	9018 537(3) [L9760]
9175.738(7)	1.06×10^{-2}	15.0	0.065(4)	$5d[1/2]_2 = 6p'[3/2]_2$	9175.736(3) [L9760]
9223.986(5)	2.41×10^{-1}	26.0	0.063(3)	$6s[3/2]_1-6p[1/2]_1$	9223.98(2) [L7293]
9292.091(9)	2.23×10^{-3}	12.5	0.053(8)	$5d[1/2]_1 - 6p'[1/2]_1$	9292.12(2) [L7293]
9337.317(20)	7.05×10^{-3}	25.8	0.056(2)	$6p[3/2]_2 - 6d[1/2]_1$	9337.32(2) [L7293]
9476.289(27)	3.47×10^{-4}	3.94	0.079(26)	$5d[3/2]_1 - 5f[3/2]_2$	9476.29(3) [L7293]
9496.002(5)	2.45×10^{-2}	16.6	0.057(2)	$6p[3/2]_2 - 6d[3/2]_2$	9496.007(6) [L9760]
9507.444(b) 9514.000(10)	4.44×10^{-4}	11.9	0.067(9)	$5a[1/2]_0 - 6p'[1/2]_1$ $5d[2/2]_0 - 5f[5/2]_1$	9507.483(21) [L4739]
9534 999(8)	6.66×10^{-4}	9.20 10.5	0.007(9)	$5u_{13/2}_{1-3/[3/2]_{2}}$ $6v_{13/2}_{1-6d[1/2]_{2}}$	9534 976(21) [L4/39]
9752.440(5)	4.04×10^{-3}	20.1	0.052(2)	$6p[3/2]_1 - 6d[3/2]_2$	9752.406(22) [L4739]
9812.430(8)	5.87×10^{-4}	11.1	0.045(7)	$6p[3/2]_2 - 6d[7/2]_3$	9812.433(22) [L4739]
9873.403(8)	2.36×10^{-3}	9.21	0.072(6)	$5d[1/2]_1-6p'[1/2]_0$	9873.378(22) [L4739]
9891.065(5)	1.66×10^{-2}	40.3	0.042(2)	$5d[7/2]_{3}-4f[9/2]_{4}$	9891.089(23) [L4739]
9913.194(5)	2.20×10^{-3}	18.8	0.044(3)	$6p[1/2]_0 - 6d[3/2]_1$	9913.205(23) [L4739]
9973.613(7)	2.43×10^{-3}	7.98	0.056(5)	$5d[7/2]_3 - 4f[7/2]_3$	9973.602(23) [L4739]
9973.691(10)	1.91×10^{-3}	4.44	0.078(7)	$5d[7/2]_3 - 4f[7/2]_4$	9973.602(23) [L4739]

Table 2 (continued).					
$v_{\nu_{i}}$ (cm ⁻¹)	I_{ν_i}	SNR	FWHM	Identification	Other work
KI · ·	(arb. u.)		(cm ⁻¹)		(if any)
10030.785(12)	1.21×10^{-4}	4.84	0.024(11)	$6p[3/2]_2-6d[5/2]_2$	10030.782(23) [L4739]
10074.645(7)	7.86×10^{-1}	7.00	0.110(3)	$6s[3/2]_1 - 6p[5/2]_2$	10074.6342(71) [L7292]
10201.602(14)	1.07	5.24	0.125(11)	$6s[3/2]_2 - 6p[1/2]_1$	10201.5997(21) [L7292]
10287.226(5)	9.00×10^{-3}	61.5	0.044(2)	$6p[3/2]_1 - 6d[5/2]_2$	10287.193(24) [L4739]
10305.415(8)	8.08×10^{-4}	11.6	0.060(7)	$6p[5/2]_2 - 6d[3/2]_2$	10305.400(24) [L4739]
10322.102(5)	1.10×10^{-2}	13.3	0.045(2)	$6p[3/2]_2 - 6d[5/2]_3$	10322.073(25) [L4739]
10429.982(10)	6.76×10^{-4}	10.9	0.055(8)	$6p[5/2]_2 - 6d[1/2]_1$	10429.955(25) [L4739]
10508.628(5)	3.29×10^{-2}	20.0	0.043(2)	$6p[5/2]_2 - 6d[7/2]_4$	10508.6318(22) [L7292]
10526.696(6)	1.79×10^{-3}	20.3	0.055(4)	$5d[3/2]_2 - 4f[3/2]_2$	10526.676(25) [L4739]
10584.342(5)	6.11×10^{-3}	72.9	0.043(2)	$5d[3/2]_2 - 4f[5/2]_2$	10584.328(26) [L4739]
10587.308(14)	3.19×10^{-4}	5.64	0.048(12)	$5d[3/2]_2 - 4f[5/2]_2$	10587.309(26) [L4739]
10588.686(20)	3.82×10^{-4}	4.92	0.069(19)	$6p[5/2]_2 - 6d[3/2]_2$	10588.677(26) [L4739]
10621.828(5)	3.61×10^{-3}	53.6	0.042(2)	$6p[5/2]_2 - 6d[7/2]_2$	10621.809(26) [L4739]
10664.024(5)	1.30×10^{-2}	17.6	0.044(2)	$5d[7/2]_4 - 4f[9/2]_5$	10664.014(26) [L4739]
10664.880(14)	3.14×10^{-4}	5.71	0.039(12)	$5d[7/2]_4 - 4f[9/2]_4$	10664.856(27) [L4739]
10742.100(11)	2.07×10^{-3}	13.5	0.120(10)	$6s'[1/2]_1 - 7p[1/2]_1$	10742.069(27) [[.4739]
10747.508(6)	1.29×10^{-3}	22.2	0.051(4)	$5d[7/2]_4 - 4f[7/2]_4$	10747.485(27) [L4739]
10840.189(12)	1.69×10^{-4}	5.14	0.034(10)	$6n[5/2]_{2}-6d[5/2]_{2}$	10840.201(27) [L4739]
10853.160(8)	6.83×10^{-4}	10.1	0.051(7)	5d[1/2], -4f[3/2],	10853.158(27) [L4739]
10862.829(9)	1.37×10^{-3}	11.1	0.075(7)	$5d[1/2]_1 - 4f[3/2]_2$	10862.805(27) [L4739]
10905.083(5)	1.22×10^{-2}	28.4	0.045(2)	$6n[5/2]_{2} - 6d[7/2]_{2}$	10905.083(27) [L4739]
10910 879(6)	2.88×10^{-1}	8 44	0.096(2)	$6s[3/2]_{2} - 6n[3/2]_{3}$	10910 8763(6) [L7292]
10923 427(18)	4.18×10^{-4}	5.58	0.073(16)	$5d[1/2]_{-}=4f[5/2]_{-}$	10923 432(27) [L4739]
10990 697(10)	5.35×10^{-4}	8 76	0.050(8)	$5d[5/2]_{-5}f[7/2]_{-5}$	10990 670(28) [14739]
11052 253(5)	2.41×10^{-1}	20.4	0.080(3)	$6s[3/2]_{-}=6n[5/2]_{-}$	11052 2523(6) [L7292]
11068 504(7)	7.85×10^{-4}	12.1	0.053(5)	$5d[1/2]_2 - 4f[3/2]_2$	11068 486(28) [L4739]
11076 129(13)	4.83×10^{-4}	6.92	0.065(11)	$6n[3/2]_{-}=6d[3/2]_{-}$	11076 089(28) [L4739]
11123 463(5)	2.07×10^{-3}	23.7	0.051(3)	$6n[5/2]_{2} = 6d[5/2]_{2}$	11123 424(12) [[4739]
11120.100(0)	8.63×10^{-4}	11.3	0.052(7)	$6p[5/2]_2 = 6d[5/2]_2$	11131 500(21) [14739]
11166 637(23)	2.87×10^{-4}	2 66	0.038(22)	$6s'[1/2]_{3} = 7n[5/2]_{3}$	11166 649(21) [14739]
11167 310(5)	1.34×10^{-1}	16.3	0.076(3)	6s[3/2] - 6n[3/2]	11167 3002(6) [17202]
11194 087(5)	3.02×10^{-3}	21.1	0.059(3)	6s'[1/2] = 6n'[3/2]	11194 094(21) [14739]
11221 880(5)	2.69×10^{-3}	29.4	0.053(3)	$6n[1/2]_1 = 6d[1/2]_1$	11221 863(21) [[4739]
11221.000(0)	5.50×10^{-3}	22.1	0.057(2)	$6p[1/2]_1 = 6d[1/2]_0$	11280 630(22) [14739]
11335 520(11)	4.16×10^{-1}	6.42	0.122(9)	$6s[3/2]_{-6n}[5/2]_{-6n}[5/2]_{-6n}$	11335 5135(6) [L7292]
11414 773(11)	4.99×10^{-4}	5.97	0.054(10)	$6n[5/2]_{2} - 6d[5/2]_{2}$	11414 736(22) [[4739]
11439 323(5)	2.89×10^{-3}	11.6	0.055(2)	$6p[1/2]_2 = 6d[3/2]_3$	11439 328(3) [L7292]
11475 949(7)	2.00×10^{-4}	10.4	0.025(5)	$5d[5/2]_{-} = 5f[5/2]_{-}$	11475 875(22) [[4739]
11495 307(11)	3.22×10^{-4}	7 21	0.041(9)	5d[5/2] = 5f[7/2]	11495 246(22) [14739]
11888 488(7)	1.79×10^{-2}	13.7	0.081(5)	$6s[3/2]_{-}=6n[3/2]_{-}$	11888 4857(7) [L7292]
11977 314(5)	6.10×10^{-3}	60.2	0.058(3)	$6s'[1/2]_2 - 6p'[3/2]_1$	11977 3164(7) [17292]
12073 808(7)	7.75×10^{-2}	6.03	0.080(2)	$6s[3/2]_1 - 6n[1/2]_2$	12073 8065(7) [L7292]
12093 667(13)	7.64×10^{-4}	6 79	0.057(12)	$6s'[1/2]_{-6p'[1/2]_{0}}$	12073.6003(7) [17292] 12093 665(3) [17292]
12144 927(7)	1.65×10^{-1}	30.4	0.115(5)	$6s[3/2]_{-6n}[3/2]_{-6n}$	12073.003(3) [E7292]
12182 349(9)	1.55×10^{-3}	9.82	0.081(8)	6s'[1/2] - 6n'[3/2]	12137.3107(7) [17292]
12407 745(21)	3.95×10^{-4}	5.01	0.070(19)	5d[7/2] = 5f[9/2]	12407 758(3) [L7202]
	5.75 × 10	3.01	0.07 0(17)	5417 213-57 [7/2]4	12 107 .7 00(0) [1/2/2]



Fig. 5. Normal probability plot of reduced residuals from two datasets: (i) all dipole-allowed transitions listed at NIST database [11] and (ii) our linelist. The most of both data points align relatively close to the straight line with a unit slope. This implies that our R_i values exhibit a distribution close to the normal distribution.

n, which is whole amount of used transitions. For the measurements to be consistent with the given identifications it would be expected that

the root mean square (RMS) value of the R_i values is close to or less than 1. Generated normal probability plot on Fig. 5 shows that R_i values

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Table 3

Refinement of Xe 6 g, 6h, 7h, 7i levels. The complete list of re-optimized levels with uncertainties and comparison with the NIST ASD [11] values is included as a supplementary online material.

Level	Energy (cm ⁻¹)
$7i\left[\frac{9}{2}\right]_5$	95592.28(5)
$7i\left[\frac{9}{2}\right]_4$	95592.29(7)
$7i\left[\frac{15}{2}\right]_8$	95592.82(4)
$7i\left[\frac{15}{2}\right]_7$	95592.82(5)
$7i\left[\frac{11}{2}\right]_6$	95594.515(20)
$7i\left[\frac{11}{2}\right]_5$	95594.524(24)
$7i\left[\frac{13}{2}\right]_7$	95594.99(3)
$7i\left[\frac{13}{2}\right]_6$	95595.00(4)
$7h\left[\frac{7}{2}\right]_3$	95590.33(6)
$7h\left[\frac{7}{2}\right]_4$	95590.39(5)
$7h\left[\frac{13}{2}\right]_7$	95591.382(18)
$7h\left[\frac{13}{2}\right]_6$	95591.384(20)
$7h\left[\frac{9}{2}\right]_{5}$	95594.068(28)
$7h\left[\frac{9}{2}\right]_4$	95594.077(31)
$6h\left[\frac{7}{2}\right]_4$	94779.573(10)
$6h\left[\frac{7}{2}\right]_3$	94779.584(11)
$6h\left[\frac{13}{2}\right]_7$	94781.219(15)
$6h\left[\frac{13}{2}\right]_6$	94781.221(13)
$6h\left[\frac{9}{2}\right]_5$	94785.474(12)
$6h\left[\frac{9}{2}\right]_4$	94785.483(14)
$6h\left[\frac{11}{2}\right]_6$	94787.096(12)
$6h\left[\frac{11}{2}\right]_5$	94787.106(17)
$6g\left[\frac{5}{2}\right]_2$	94771.528(6)
$6g\left[\frac{5}{2}\right]_3$	94771.593(5)
$6g\left[\frac{11}{2}\right]_6$	94775.0312(49)
$6g\left[\frac{11}{2}\right]_5$	94775.0337(48)
$6g\left[\frac{7}{2}\right]_4$	94782.2095(52)
$6g\left[\frac{7}{2}\right]_3$	94782.222(4)
$6g\left[\frac{9}{2}\right]_4$	94785.845(6)
$6g\left[\frac{9}{2}\right]_5$	94785.852(6)

are close to the normal statistical distribution (slope is 1.13, the vertical offset from the origin is 0.04).

When generating the normal probability plot in Fig. 5, we excluded the lines that solely determine one of the levels. We also excluded duplicate lines measured in different studies, selecting the value with the smaller uncertainty. It should also be noted that we used revised estimates of uncertainties for many of the NIST ASD lines, most notably Humphreys and Meggers [6], Humphreys and Kostkowski [7], Mishra et al. [9]. The supplementary table with the full line list (LOPT input file) contain these revised uncertainties.

The distribution of the residuals R_i , shows that the system of Xe I levels obtained in our optimization procedure is internally consistent within $\simeq 0.02$ cm⁻¹. The resulting complete list of re-optimized levels (actually, the LOPT level output file) with uncertainties and comparison with the NIST ASD [11] values is included as a supplementary online material. Table 3 contains newly reported Rydberg levels that belong to

the 6 g, 6 h, 7 h, 7i configurations only. Unfortunately, we were unable to resolve all components of the 7 h multiplet. The reason is probably that the transitions involving 7h[11/2] are weak and/or blended by other multiplet components. As a result, only 6 out of 8 lines of the 7 h multiplet are included in Table 3.

LOPT code is able to return different values of level uncertainties [38, Eqs. (26), (31), (32)]. The uncertainty D_2 relative to the ground level, is frequently used. However, in rare gases the excited levels are usually measured much more accurately relative to the lowest excited level in this case, $6s[3/2]_2$. Thus, all uncertainties (including the ground level) specified in Table 3 are given for the intervals from this base level. The uncertainties of excitation energies from the ground level must be calculated as sums in quadrature of the tabulated uncertainty and that of the ground level (0.004 cm⁻¹ in this case).

4. Conclusion

Although the neutral xenon (Xe I) spectra have been studied for a long time, an important part of mid-infrared (MIR) spectral region has not been studied in precision laboratory measurements. As a result, no high-quality spectroscopic data for Xe I are available in the literature (for instance, the NIST ASD [11] lacks experimental lines with wavenumbers less than 1800 cm⁻¹). However, this spectral range can be of interest for infrared astronomy as well as for infrared lasing [47, 48]; therefore, providing new spectroscopic data for Xe in the infrared domain is important.

This study attempts to fill the gap in the high-resolution MIR spectra of Xe I. Most of the Xe I spectrum measurements were performed more than a half century ago. In this study, we remeasured the Xe I emission spectrum within the wavelength range of $0.7-14 \ \mu\text{m}$ (corresponding to the wavenumber range of $700-14,000 \ \text{cm}^{-1}$). 335 lines of atomic xenon are reported, and 111 of them are observed for the first time. No high-resolution spectra have previously been available for the spectral region below 2000 cm⁻¹ (wavelength longer than 5 μ m). The most prominent lines in this region are due, as a rule, to transitions from Rydberg levels with high orbital momentum, l = 4..6 (g-, h-, and i-levels). After combining all available Xe I lines in a least-square optimization procedure, we have obtained an updated Xe I level system, which now includes the newly observed Rydberg 6 g, 6 h, 7 h, and 7i levels. Our improved system of Xe I levels is internally consistent within $\simeq 0.02 \ \text{cm}^{-1}$.

CRediT authorship contribution statement

S. Civiš: Supervision, Resources, Project administration, Methodology, Formal analysis, Data curation, Conceptualization. **E.M. Zanozina:** Writing – review & editing, Writing – original draft, Visualization, Validation, Formal analysis, Data curation. **P. Kubelík:** Validation, Software, Resources, Project administration, Methodology, Formal analysis, Data curation. **V.E. Chernov:** Writing – review & editing, Writing – original draft, Supervision, Formal analysis. **A. Pastorek:** Formal analysis, Data curation. **M. Ferus:** Supervision, Project administration, Funding acquisition.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data availability

Data will be made available on request.

Acknowledgments

We wish to thank Alexander E. Kramida from National Institute of Standards and Technology for helpful recommendations and advices on processing all data for our compilation, which significantly enhanced the accuracy and reliability of our work.

This work was supported by the ERDF/ESF "Centre of Advanced Applied Sciences" (no. CZ.02.1.01/0.0/0.0/16_019/0000778) (S.C.). P.K. acknowledges the support from the Czech Science Foundation (grant no. 20-10591J). V.Ch. acknowledges the support from the Ministry of Science and Higher Education of Russian Federation (grant number FZGU-2020-0035).

Appendix A. Supplementary data

Supplementary material related to this article can be found online at https://doi.org/10.1016/j.jqsrt.2024.108939.

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